

Kittitas County CDS

The Outpost at Lake Cle Elum

Kittitas County, WA

Traffic Impact Analysis

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FINDINGS/ CONCLUSIONS

This traffic impact analysis (TIA) has been prepared for the proposed *Outpost at Lake Cle Elum* project located at 510 Sandelin Lane in Kittitas County, WA.

Project Proposal. The proposed *Outpost at Lake Cle Elum* project would include the development of up to 50 recreational homes/cabins. The existing site is comprised of four parcels and includes one single-family home that may be repurposed with the proposed project. For the purposes of this analysis, no credit was assumed for the existing use. Vehicular access to the proposed development is proposed via one new full access driveway on Salmon La Sac Road.

Time Period for Traffic Analysis. Based on scoping discussions with Kittitas County and the Washington State Department of Transportation (WSDOT), the daily variation in traffic on roadways in the vicinity of the *Outpost at Lake Cle Elum* site is generally higher on Fridays and weekends during the peak summer season. This is a result of the use of second homes located in the vicinity of the proposed project along Cle Elum Lake, other recreational amenities in the area, and the higher level of traffic on SR 903 on Fridays and weekends during the peak summer months. As a result, this traffic impact analysis evaluates conditions during the Friday PM peak hour.

Trip Generation. The proposed *Outpost at Lake Cle Elum* project is anticipated to generate 56 new trips during the Friday PM peak hour (33 entering, 23 exiting).

Intersection Level of Service. Friday PM peak hour LOS analyses were conducted at five (5) unsignalized off-site study intersections: four (4) in Kittitas County and one (1) in the City of Roslyn. The results of the LOS analyses indicated that all turn movements at the stop-controlled study intersections are expected to meet the applicable level of service (LOS) standard during the Friday PM peak hour in 2023 without or with the proposed *Outpost at Lake Cle Elum* project. The minimum LOS standard at all study intersections is LOS C.

Roadway Corridor Level of Service. Friday PM peak hour roadway corridor LOS analyses were conducted for the Salmon La Sac Road corridor between Brekenridge Drive and Wadsworth Loop (southern). The results of the corridor LOS analyses indicated that the corridor is expected to meet the applicable LOS standard in year 2023 without or with the proposed *Outpost at Lake Cle Elum* project. Kittitas County minimum LOS standard for roadway corridors in rural areas is LOS C.

Site Access Level of Service. Per scoping discussions with County staff, Friday PM peak hour LOS and queuing analyses were conducted at the proposed site access driveway location on Salmon La Sac Road. The results of the analyses indicated that the turning movements at the proposed site access driveway on Salmon La Sac Road are anticipated to operate at LOS A with minimal queuing with the proposed project during the Friday PM peak hour.

Sight Distance. Sight distance evaluations were conducted in the vicinity of the proposed site access driveway on Salmon La Sac Road at Wadsworth Loop (northern) and Crawford. Based on field measurements, there are no known constraints on Salmon La Sac Road between Wadsworth Loop (northern) and Crawford that would prevent sight distance requirements from being met at the proposed site access location. Any proposed landscaping, signage, and street furnishings at the proposed site driveway location would need to be positioned in such a way that would avoid creating a sightline obstruction within the sight triangles. Any street trees or other vegetation within the sight triangles would also need to be trimmed to maintain clear visibility.

INTRODUCTION

This traffic impact analysis (TIA) documents the traffic impacts associated with the proposed *Outpost* at Lake Cle Elum project located at 510 Sandelin Lane in Kittitas County, WA. A project vicinity map is provided in **Figure 1**.

Project Description

The proposed *The Outpost at Lake Cle Elum* project would include the development of up to 50 recreational homes/cabins. The existing site is comprised of four parcels and includes one single-family home that may be repurposed with the proposed project. For the purposes of this analysis, no credit was assumed for the existing use. Vehicular access to the proposed development is proposed via one new full access driveway on Salmon La Sac Road. For this analysis, a horizon year of 2023 was used. A preliminary site plan is included in **Figure 2**.

Project Approach

The specific scope of work used in the evaluation of the traffic impacts of the proposed *Outpost at Lake Cle Elum* project were confirmed through scoping discussions with Kittitas County and WSDOT staff. To analyze the traffic impacts from the proposed *Outpost at Lake Cle Elum* project, the following tasks were undertaken:

- Assessed existing conditions through field reconnaissance and reviewed existing planning documents.
- Described existing roads, pedestrian facilities, and transit facilities in the project vicinity.
- Documented the latest 3-year collision history at the study intersections and project frontage.
- Documented existing (2022) traffic volumes and intersection LOS at off-site study intersections during the Friday PM peak hour.
- Documented existing (2022) Friday PM peak hour traffic volumes and LOS for the Salmon La Sac Road corridor between Brekenridge Drive and Wadsworth Loop (southern).
- Documented future planned roadway improvements in the project vicinity.
- Developed trip generation estimates for Friday daily, AM, and PM peak hour conditions based on the proposed land use.
- Documented trip distribution and assignment of Friday PM peak hour project-generated traffic.
- Documented traffic forecasts and assumptions for year 2023 Friday PM peak hour conditions at off-site study intersections without and with the proposed development.
- Analyzed Friday PM peak hour LOS for future year 2023 conditions without and with the proposed development at off-site intersections and along the Salmon La Sac Road corridor between Brekenridge Drive and Wadsworth Loop (southern).
- Assessed operations at the proposed site access location, including LOS and queuing during Friday PM peak hour conditions.
- Evaluated available sight distances along Salmon La Sac Road.
- Documented proposed traffic mitigation.



Primary Data and Information Sources

- 2022 Friday PM Peak Hour traffic counts (IDAX).
- Kittitas County 2023-2028 6-Year Transportation Improvement Plan (Adopted December 7, 2021).
- Kittitas County Transportation Element 2018.
- Institute of Transportation Engineers (ITE) Trip Generation Manual, 11th Edition, 2021;
- Transportation Research Board (TRB), Highway Capacity Manual (HCM), 6th Edition, 2016.
- WSDOT 2019-2021 Collision Data.
- Florida Department of Transportation (FDOT), 2020 Quality/ Level of Service Handbook.
 June 2020.



Figure 1: Project Site Vicinity



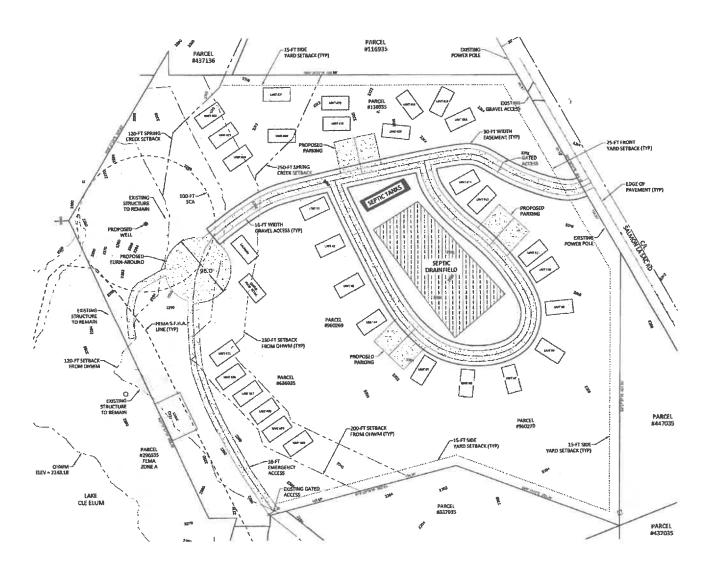


Figure 2: Preliminary Site Plan





EXISTING CONDITIONS

Study Area

The existing transportation study area and roadway network providing access to the *Outpost at Lake Cle Elum* site is shown on **Figure 1**. The off-site study intersections evaluated in this transportation analysis were identified and agreed upon by Kittitas County and WSDOT as part of the traffic scoping process. The five off-site study intersections are as follows (see also **Figure 3**):

- 1. Salmon La Sac Road / Spring Creek Road
- 2. Salmon La Sac Road / Wadsworth Loop (northern)
- 3. Salmon La Sac Road / Crawford Street
- 4. Salmon La Sac Road / Sandelin Lane
- 5. W 1st Street (SR 903) / Pennsylvania Ave

Roadway Network

The primary vehicle travel route to and from the site is via Salmon La Sac Road and described below in more detail:

Salmon La Sac Road is a two-way, rural minor collector that borders Cle Elum Lake in Kittitas County, WA. Salmon La Sac Road is a 2-lane roadway that begins at the boundary of the Wenatchee National Forest at Mile Post 10.0, east of Cle Elum Lake, where State Route 903 (SR 903) begins. Along the project frontage, Salmon La Sac Road has a posted speed limit of 35 miles per hour (mph). There are no curb, gutter, sidewalk, illumination, or pedestrian facilities within the immediate vicinity of the site along Salmon La Sac Road.

SR 903 connects from Salmon La Sac Road to the I-90/SR 970/SR 903 interchange at White Road, through the City of Ronald, Roslyn, and Cle Elum.

Transit Service

There are no existing transit services to and from the project vicinity. The closest transit service relative to the project site is located in the City of Ronald, approximately three (3) miles south of the proposed project.

Non-Motorized Transportation Facilities

There are no existing non-motorized transportation facilities in the immediate vicinity of the site. Based on traffic counts conducted at the study intersections, there is no pedestrian activity within the immediate vicinity of the site.

Collision History

Collisions at the study intersections and along Salmon La Sac Road were summarized for the most recent 3-year period from January 1, 2019 to December 31, 2021. Collision data was provided by the Washington State Department of Transportation (WSDOT). Summaries of the total, annual average, and collision type along Salmon La Sac Road are provided in **Error! Reference source not found.**. Note that there were no collisions reported at any of the off-site study intersections during the time period evaluated.

Table 1 Collision Data Summary by Type, January 1, 2019 to December 31, 2021

| | | | 1 71 | <u>Co</u> | llisior | Тур | <u>e</u> | |
|---|-------------------------------|-----------------------------|-----------|--------------------|----------|-----------|-----------|-------|
| Segment | 3-Year Total Collisions | Avg. Annual Collision | Angle (T) | Angle (Left/Right) | Rear End | Sideswipe | Ped/Cycle | Other |
| Salmon La Sac Rd Between Breckenridge Dr and Wadsworth Loop (southern) | 1 | 0.33 | 0 | 0 | 0 | 0 | 0 | 1 |

Source: WSDOT Collision Records.

Traffic Volumes

Existing Friday PM peak hour traffic volumes at the study intersections were based on traffic counts conducted in August 2022. The PM peak hour represents the highest one-hour time period between 4:00 and 6:00 PM. **Appendix A** includes the existing peak hour traffic count sheets.

The 2022 existing Friday PM peak hour traffic volumes at the study intersections are illustrated in **Figure 3**. The detailed peak hour turning movement count sheets are provided in **Appendix A**.

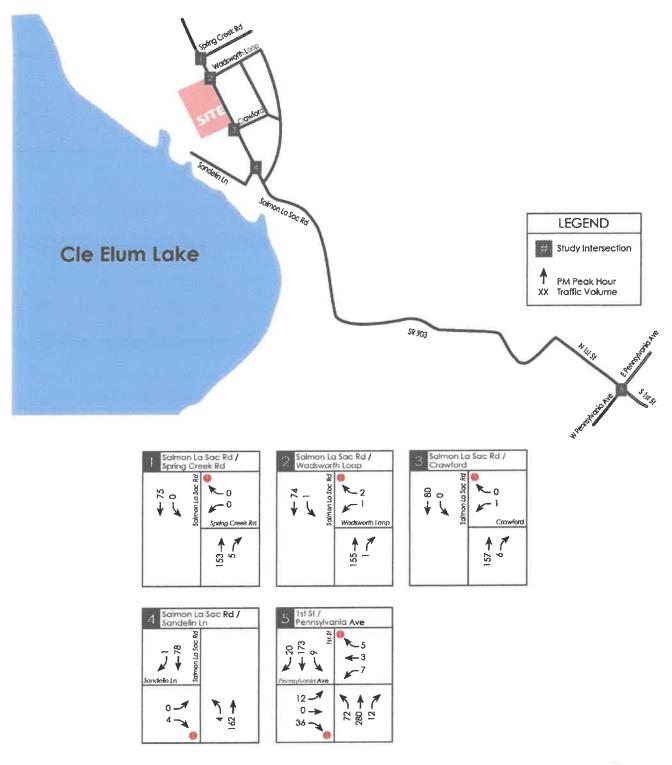


Figure 3: 2022 Existing Friday PM Peak Hour Traffic Volumes



Existing Intersection Level of Service

An existing Friday PM peak hour level of service (LOS) analysis was conducted at the off-site study intersections. LOS generally refers to the degree of congestion on a roadway or intersection. It is a measure of vehicle operating speed, travel time, travel delays, and driving comfort. A letter scale from A to F generally describes intersection LOS. At signalized intersections, LOS A represents free-flow conditions (motorists experience little or no delays), and LOS F represents forced-flow conditions where motorists experience an average delay in excess of 80 seconds per vehicle.

The LOS reported for signalized intersections and stop controlled intersections represents the average control delay (sec/veh) and can be reported for the overall intersection, for each approach, and for each lane group or movement (additional v/c ratio criteria apply to lane group or movement LOS only). The LOS reported at two-way stop-controlled intersections is based on the average control delay and can be reported for each controlled minor approach, controlled minor lane group, and controlled major-street movement (additional v/c ratio criteria apply to lane group or movement LOS only).

Table 2 outlines the current HCM 6^{th} Edition LOS criteria for signalized and unsignalized intersections based on these methodologies.

Table 2
LOS Criteria for Signalized and Stop-Controlled Intersections¹

| 200 Cilicità ioi | | | 10.1010.1.1.17 | |) (C | | | |
|---------------------------|------------------|-------------------------|----------------------------|------------|-------------------------|--|--|--|
| SIGNALIZ | ZED INTERSECTION | <u>ons</u> | UNSIGNALIZED INTERSECTIONS | | | | | |
| | LOS by Vo | olume-to | | LOS by V | olume-to | | | |
| Tipered In a second | Capacity (V | //C) Ratio ² | | Capacity (| V/C) Ratio ³ | | | |
| Control Delay | | | Control Delay | | | | | |
| (sec/veh) | ≤ 1.0 | > 1.0 | (sec/veh) | ≤ 1.0 | > 1.0 | | | |
| ≤ 10 | Α | F | ≤ 10 | Α | F | | | |
| $> 10 \text{ to } \le 20$ | В | F | $> 10 \text{ to } \le 15$ | В | F | | | |
| > 20 to ≤ 35 | С | F | $> 15 \text{ to } \le 25$ | С | F | | | |
| > 35 to ≤ 55 | D | F | > 25 to ≤ 35 | D | F | | | |
| > 55 to ≤ 80 | E | F | $> 35 \text{ to} \le 50$ | E | F | | | |
| > 80 | F | F | > 50 | F | F | | | |

¹⁾ Source: Highway Capacity Manual, Transportation Research Board, 6th Edition, 2016.

The analysis was conducted using the methodology and procedures outlined in the 6^{th} Edition of the Highway Capacity Manual and Synchro 11 methodology/traffic analysis software.

Based on the Kittitas County and WSDOT LOS standards, the LOS standard is LOS C at all study intersections.

The 2022 PM LOS analysis results for the off-site study intersections are summarized in **Table 3**. The 2022 existing detailed LOS worksheets are included in **Appendix B**.

²⁾ For approach-based and intersection-wide assessments at signals, LOS is defined solely by control delay.

³⁾ For two-way stop-controlled intersections, the LOS criteria apply to each lane on a given approach and to each approach on the minor street. LOS is not calculated for major-street approaches or for the intersection as a whole at two-way stop controlled intersections. For approach-based and intersection-wide assessments at all-way stop controlled intersections, LOS is solely defined by control delay.

Table 3
2022 Existing PM Peak Hour LOS Summary

| | 20 |)22 Existing |
|---|-----|--------------|
| Study Intersections | LOS | Delay (sec |
| Stop-Controlled Intersections: | | |
| 1. Salmon La Sac Rd / Spring Creek Rd | | |
| Westbound Approach | Α | 0.0 |
| Southbound Left-Turn | Α | 0.0 |
| 2. Salmon La Sac Rd / Wadsworth Loop | | |
| Westbound Approach | Α | 9.3 |
| Southbound Left-Turn | Α | 7.5 |
| 3. Salmon La Sac Rd / Crawford Rd | | |
| Westbound Approach | В | 10.1 |
| Southbound Left-Turn | Α | 0.0 |
| 4. Salmon La Sac Rd / Sandelin Ln | | |
| Eastbound Approach | Α | 9.0 |
| Northbound Left-Turn | Α | 7.4 |
| 5. W 1st St (SR 903) / Pennsylvania Ave | | |
| Eastbound Approach | В | 12.9 |
| Westbound Approach | С | 16.1 |
| Northbound Left-Turn | Ā | 8.0 |
| Southbound Left-Turn | A | 8.2 |

As shown in **Table 3**, all turn movements at the stop-controlled study intersections currently meet the applicable level of service (LOS) standard during the Friday PM peak hour.

Existing Corridor Level of Service

An existing PM peak hour LOS analysis was conducted for the Salmon La Sac Road (SR 903) corridor between Brekenridge Drive and Wadsworth Loop (southern). Consistent with the methodology described in Kittitas County *Transportation Element 2018*, the corridor operations were evaluated and assigned an LOS grade based on corridor LOS definitions from the Florida Department of Transportation's (FDOT) *2020 Quality/ Level of Service Handbook*. The detailed LOS definitions used for the analysis is included in **Appendix C**. A summary of the corridor LOS analysis for the year 2022 is shown in **Table 4** below.

Table 4
2022 Existing PM Corridor LOS Summary

| | 2022 Existing | | | | | | |
|--|------------------------------|--|-----|--|--|--|--|
| Roadway Segment | Peak Hour Two- Way Volume | Maximum Service Volume ¹ | LOS | | | | |
| Salmon La Sac Rd (Breckenridge Dr to S Wadsworth Loop) | 248 | 854 | С | | | | |

Notes:

As shown in **Table 4**, the Salmon La Sac Road corridor between Breckenridge Drive to S Wadsworth Loop currently meets the applicable level of service (LOS) standard. Kittitas County minimum corridor LOS standard for rural areas is LOS C.

¹ Based on FDOT's LOS definition for rural undeveloped areas and developed areas less than 5,000 population, the adjusted maximum service volume based on the LOS standard of C is 854 vehicles per hour.

FUTURE CONDITIONS

The following section describes planned transportation improvements in the project vicinity, new trips generated by the proposed development, distribution and assignment of new project trips to the study area, projected future traffic volumes without and with the project, intersection level of service, and identification of transportation mitigation to offset impacts.

Planned Transportation Improvements

A review of Kittitas County's 2023-2028 6-Year Transportation Improvement Plan and Transportation Element 2018 showed that there are no planned transportation improvement projects by the County in the project vicinity.

Project Trip Generation

Full buildout of the proposed project would include the development of up to 50 recreational homes/cabins. The existing site is comprised of four parcels and includes one single-family home that may be repurposed with the proposed project. For the purposes of this analysis, no credit was assumed for the existing use. Trip generation for the currently proposed *Outpost at Lake Cle Elum* project was estimated based on methodology documented in the Institute of Transportation Engineers (ITE) *Trip Generation Manual* (11th Edition, 2021) for Land Use Code (LUC) 260 (Recreational Homes).

Table 5 summarizes the resulting new Friday daily, AM peak hour, and PM peak hour trip generation estimates for the proposed project. Detailed trip generation calculations are provided in **Appendix D.**

Table 5
Trip Generation Summary

| | New | Trips Gene | <u>rated</u> |
|---------------------|-----|------------|--------------|
| Time Period | In | Out | Total |
| Friday Daily | 340 | 340 | 680 |
| Friday AM Peak Hour | 23 | 19 | 42 |
| Friday PM Peak Hour | 33 | 23 | 56 |

As shown in **Table 5**, the proposed *Outpost at Lake Cle Elum* project is estimated to generate 680 new Friday daily trips, with 42 new trips occurring during the Friday AM peak hour (23 in, 19 out), and 56 new trips occurring during the Friday PM peak hour (33 in, 23 out).

Project Trip Distribution and Assignment

The distribution of project trips generated by the *Outpost at Lake Cle Elum* project was estimated based on existing and anticipated traffic patterns in the vicinity of the site and confirmed with Kittitas County and WSDOT during scoping. **Table 6** summarizes the resulting general trip distribution patterns.

Table 6
Peak Hour Project Trip Distribution

| Trip Distribution |
|-------------------|
| 10% |
| 90% |
| 100% |
| |

Based on the trip distribution percentages shown in **Table 6**, the Friday PM peak hour project trips were assigned through the off-site study intersections and site access driveway. **Figure 4** illustrates the resulting distribution and assignment of Friday PM peak hour project trips through the study intersections and site access location.

Future Traffic Volumes

To estimate future year 2023 No Action (without project) traffic volumes at the study intersections, a 2.0 percent annual growth rate was applied to existing 2022 peak hour volumes to account for new development in the study area and growth in existing traffic. Consistent with scoping discussions with County staff, no other pipeline developments were considered in the analysis. The future 2023 No Action PM peak hour traffic volumes at the off-site study intersections are shown in **Figure 5**.

Adding the trip assignment from the proposed project (Figure 4) to the future 2023 No Action traffic volumes (Figure 5) results in the 2023 With Project traffic volumes at the off-site study intersections and site access driveway. The future 2023 With Project PM peak hour traffic volumes at the off-site study intersections and site access driveway are shown in Figure 6.

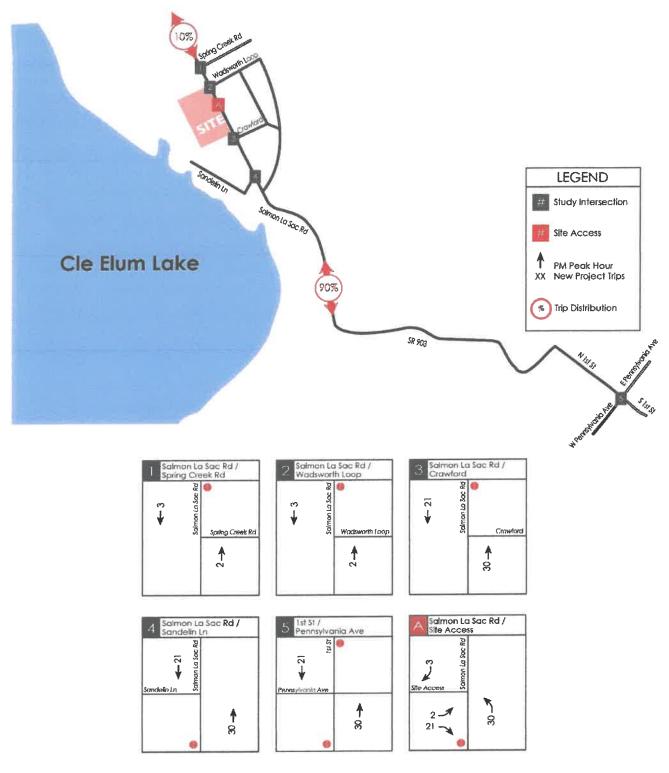


Figure 4: Friday PM Peak Hour Project Trip Assignment and Distribution



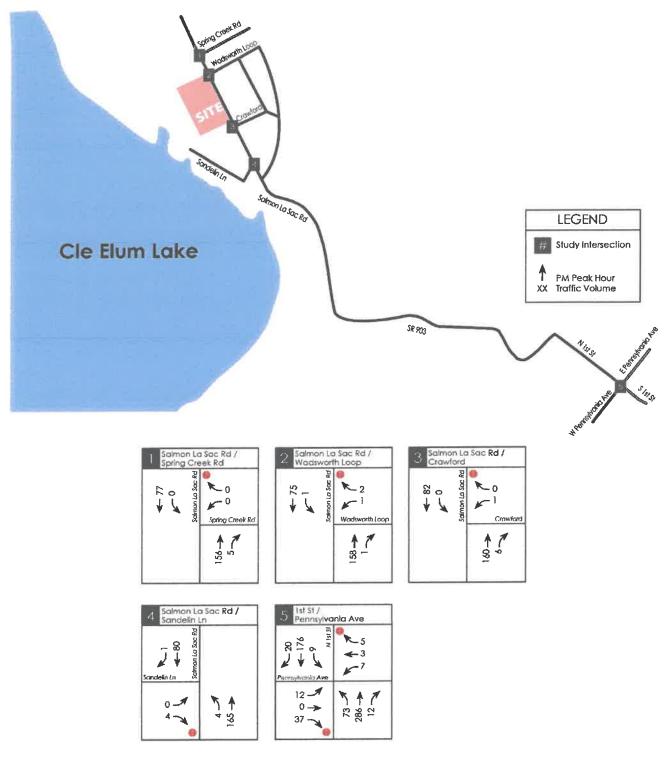


Figure 5: 2023 No Action Friday PM Peak Hour Traffic Volumes



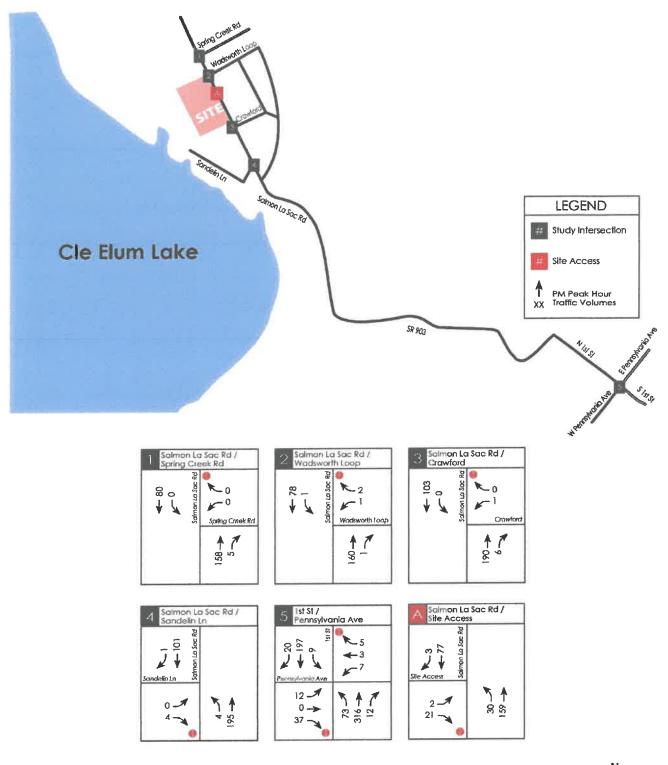


Figure 6: 2023 With Project Friday PM Peak Hour Traffic Volumes



Future Intersection Level of Service

A future year Friday PM peak hour LOS analysis was conducted at the off-site study intersections without and with the proposed project. For this analysis, a horizon year of 2023 was used. Given there are no planned transportation improvements within the study area by 2023, the roadway network assumed in the future LOS analysis was based on existing intersection geometry. The 2023 Friday PM peak hour LOS results at the off-site study intersections without and with the proposed Outpost at Lake Cle Elum project are summarized in Table 7. The detailed LOS worksheets are included in Appendix B.

Table 7

Year 2023 PM Peak Hour LOS Summary

| | 2023 N | o Action | 2023 W | 2023 With Project | | |
|---|--------|----------------|--------|-------------------|--|--|
| Study Intersection | LOS | Delay (sec) | LOS | Delay (sec) | | |
| Stop-Controlled Intersections: | | | | | | |
| 1. Salmon La Sac Rd / Spring Creek Rd | | | | | | |
| Westbound Approach | Α | 0.0 | Α | 0.0 | | |
| Southbound Left-Turn | Α | 0.0 | Α | 0.0 | | |
| 2. Salmon La Sac Rd / Wadsworth Loop | | | | | | |
| Westbound Approach | Α | 9.3 | Α | 9.3 | | |
| Southbound Left-Turn | Α | 7.5 | Α | 7.5 | | |
| 3. Salmon La Sac Rd / Crawford Rd | | | | | | |
| Westbound Approach | В | 10.2 | В | 10.6 | | |
| Southbound Left-Turn | Α | 0.0 | Α | 0.0 | | |
| 4. Salmon La Sac Rd / Sandelin Ln | | | | | | |
| Eastbound Approach | Α | 9.0 | Α | 9.2 | | |
| Northbound Left-Turn | Α | 7.4 | Α | 7.4 | | |
| 5. W 1st St (SR 903) / Pennsylvania Ave | | | | | | |
| Eastbound Approach | В | 13.0 | В | 13.5 | | |
| Westbound Approach | С | 16.3 | С | 17.3 | | |
| Northbound Left-Turn | Α | 8.0 | Α | 8.1 | | |
| Southbound Left-Turn | Α | 8.2 | Α | 8.3 | | |

As shown in **Table 7**, all turn movements at the stop-controlled study intersections are expected to meet the applicable level of service (LOS) standard during the Friday PM peak hour in 2023, without or with the proposed *Outpost at Lake Cle Elum* project.

Future Corridor Level of Service

A future PM peak hour LOS analysis was conducted for the Salmon La Sac roadway corridor between Breckenridge Drive to S Wadsworth Loop. Consistent with the methodology described in Kittitas County *Transportation Element 2018*, the corridor operations were evaluated and assigned an LOS grade based on corridor LOS definitions from the Florida Department of Transportation's (FDOT) 2020 Quality/Level of Service Handbook. The detailed LOS definitions used for the analysis is included in **Appendix C**. A summary of the corridor LOS analysis for the year 2023 is shown in **Table 8** below.

Table 8
2023 Future PM Corridor LOS Summary

| Roadway Segment | Peak Hour Two- Way Volume | Maximum Service Volume ¹ | LOS |
|--|------------------------------|---|-----|
| Salmon La Sac Rd (Breckenridge Dr to S Wadsworth Loop) | Tray volonic | TOIOTTIO | 100 |
| 2023 No Action | 253 | 854 | С |
| 2023 With Project | 309 | 854 | С |

Notes:

As shown in **Table 8**, the Salmon La Sac Road corridor between Breckenridge Drive to S Wadsworth Loop is expected to meet the applicable LOS standard in year 2023 without or with the proposed *Outpost at Lake Cle Elum* development. Kittitas County minimum corridor LOS standard for rural areas is LOS C.

Active Transportation

The majority of project trips traveling to/from the proposed *Outpost at Lake Cle Elum* project are expected to use SR 903, which connects from Salmon La Sac Road to the I-90/SR 970/SR 903 interchange at White Road, through the City of Ronald, Roslyn, and Cle Elum.

WSDOT assigned SR 903 with a Level of Traffic Stress (LTS) Rank 4 in their active transportation analysis of systemic safety and user acceptance of state highways, meaning functional gaps in active transportation may exist along the state route south of the proposed *Outpost at Lake Cle Elum* project. However, there are no current plans to implement active transportation improvements along the corridor.

Site Access Analysis

Vehicular access to the proposed development is proposed via one new full access driveway on Salmon La Sac Road (SR 903). Evaluation of the proposed site access includes peak hour LOS analysis, queuing analysis and sight distance assessments.

LOS and Queuing Analysis at Site Access

Consistent with scoping discussions with Kittitas County and WSDOT, Friday PM peak hour LOS analysis was conducted at the proposed site access driveway on Salmon La Sac Road. The estimated Friday PM peak hour traffic volumes at the proposed site access used in this analysis were shown previously in **Figure 6**. **Table 9** summarizes the 2023 Friday PM peak hour LOS results and 95th percentile queues at the proposed site access driveway on Salmon La Sac Road. The reported 95th percentile queues represent a condition that is exceeded only 5 percent of the time. The detailed LOS worksheets are included in **Appendix B**.

¹ Based on FDOT's LOS definition for rural undeveloped areas and developed areas less than 5,000 population, the adjusted maximum service volume based on the LOS standard of C is 854 vehicles per hour.

Table 9
Year 2023 With Project Peak Hour Site Access LOS and Queue Summary

| rear 2023 With Project reak hour sile Acce | PM Peak Hour | | | | | |
|--|--------------|----------------|--|--|--|--|
| Site Access Controlled Movements | LOS | Delay (sec) | 95 th % Queue (ft) ¹ | | | |
| A. Salmon La Sac Rd / Site Access | | | | | | |
| Eastbound Shared Left-Right | Α | 7.4 | < 25' | | | |
| Northbound Left-Turn | Α_ | 9.0 | < 25' | | | |

^{1.} Queues are 95th Percentile queues. <25' indicates 95th Percentile queue statistically less than 1 yeh.

As shown in **Table 9**, the individual movements entering and exiting the site are anticipated to operate at LOS A with minimal queueing (25 feet or less) with the proposed *Outpost at Lake Cle Elum* development during the Friday PM peak hour.

Sight Distance Assessment

The *Outpost at Lake Cle Elum* site access is proposed to be located south of Wadsworth Loop (northern) and north of Crawford on Salmon La Sac Road. The following summarizes the results of the sight distance assessment conducted on Salmon La Sac Road between the Wadsworth Loop (northern) and Crawford intersections.

The assessment was based on a review of Kittitas County Code (KCC) Chapter 12.4, the WSDOT Design Manual, and AASHTO's A Policy on Geometric Design of Highways and Streets, 7th Edition, 2018. Field measurements were conducted in August 2022 and the posted speed limit on Salmon La Sac Road is 35 mph in the site vicinity.

Intersection Sight Distance (ISD):

Kittitas County Code (KCC) Chapter 12.4 does not include intersection sight distance (ISD) standards. However, AASHTO standards specify a 390-foot and 335-foot minimum required sight distance for a 35-mph design speed for left and right-turning movements, respectively, onto the major roadway.

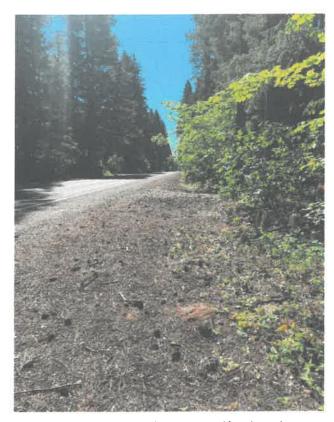
Based on AASHTO standards, ISD is measured from a point that is 14.5 feet back from the edge of the traveled way and 3.5 feet above the road surface, looking at an object height of 3.5 feet above the road surface.

Based on the field measurements conducted on Salmon La Sac Road, it appears that minimum sight distance requirements would be met for a proposed driveway location anywhere between Wadsworth Loop (northern) and Crawford.

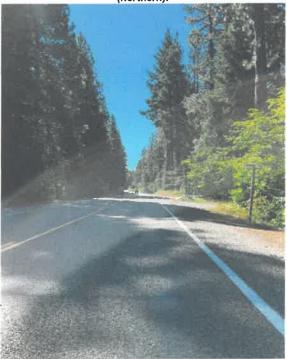
Any proposed landscaping, signage, and street furnishings would need to be positioned in such a way that would avoid creating a sight line obstruction. Any street trees or other vegetation within the sight triangles would also need to be trimmed to maintain clear visibility.

The proposed *Outpost at Lake Cle Elum* site access driveway at Salmon La Sac Road should be designed to meet the Road Design Criteria outlined in Kittitas County Code (KCC) Chapter 12.4.

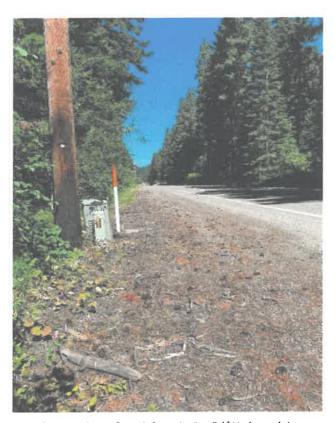
Photos looking to the northwest and southeast along Salmon La Sac Road from both the Wadsworth Loop (northern) and Crawford intersections are shown next.



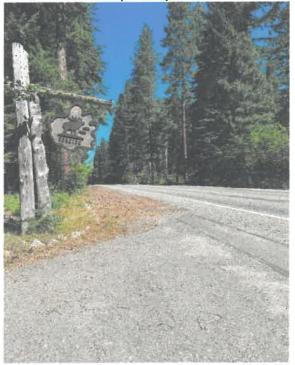
Looking Southeast from Salmon La Sac Rd/Wadsworth Loop (northern).



ISD looking Southeast from Salmon La Sac Rd/Crawford



Looking Northeast from Salmon La Sac Rd/Wadsworth Loop (northern).



ISD looking Northeast from Salmon La Sac Rd/Crawford

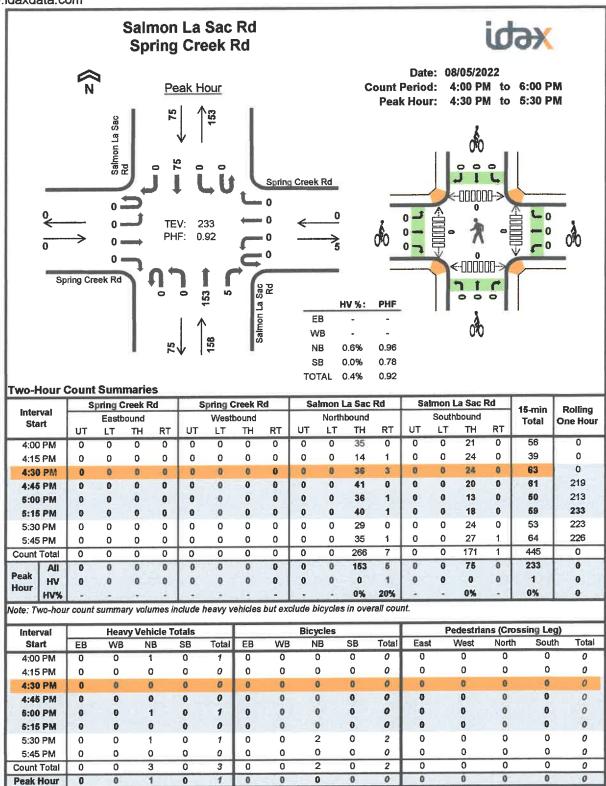
Stopping Sight Distance

Kittitas County standards specify a 250-foot minimum required stopping sight distance for a road with a 35-mph posted speed limit. Stopping sight distance was field measured based on an object height of 2.0 feet above the road surface and a driver's eye height of 3.5 feet above the road surface.

Based on field measurements, the available SSD for a vehicle traveling either northbound or southbound on Salmon La Sac approaching the proposed access driveway location exceeds 250 feet, meeting Kittitas County requirements.

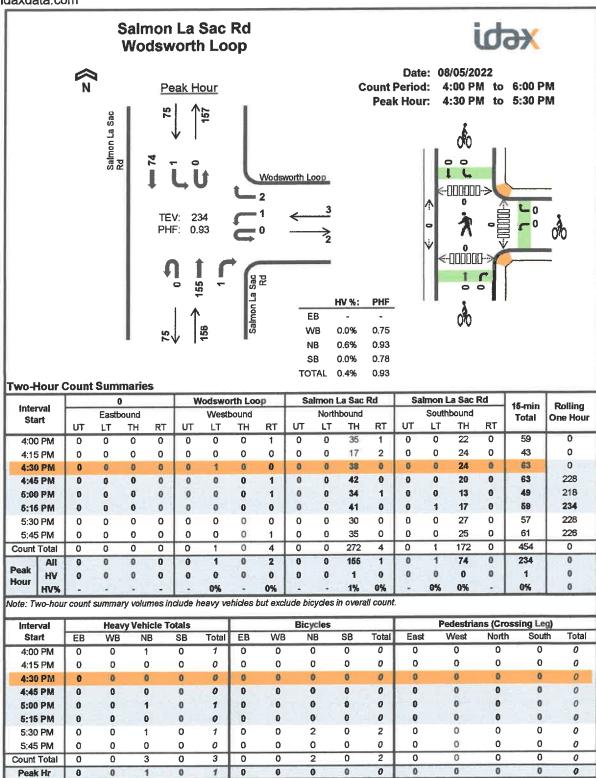
Appendix A

Traffic Count Data



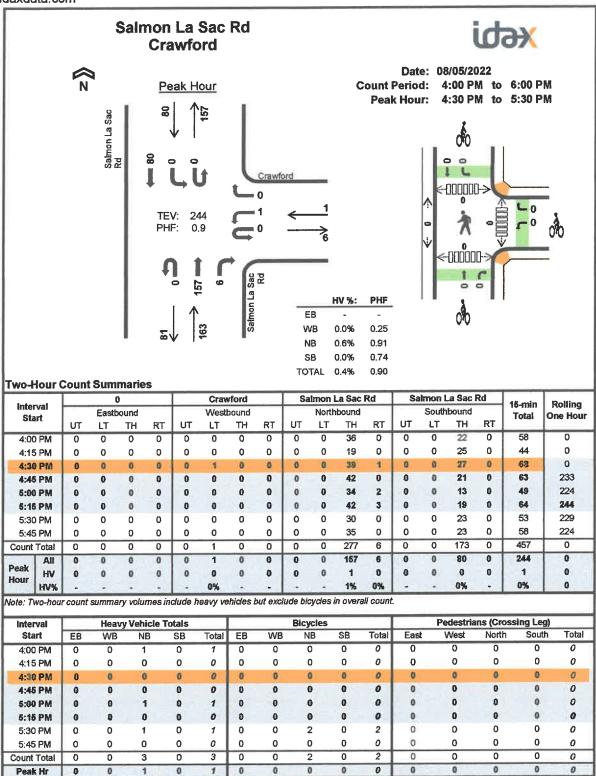
| | Spring Creek Rd | | | | Spring Creek Rd Westbound | | | Sa | Salmon La Sac Rd | | | Salmon La Sac Rd | | | | 15-min | Rolling | |
|-------------------|-----------------|----|----|------------|------------------------------|----|----|------------|------------------|----|----|------------------|----------|----|----|--------|---------|---|
| Interval Start | Eastbound | | | Northbound | | | | Southbound | | | | Total | One Hour | | | | | |
| Start | UΤ | LT | TH | RT | UT | LT | TH | RT | UΥ | LT | TH | RT | UT | LT | TH | RT | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 3 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 |

| | Spri | ing Cree | k Rd | Spri | ing Cree | k Rd | Salm | on La Sa | ac Rd | Salm | on La Sa | ac Rd | 15-min | Rolling |
|-------------------|------|----------|------|------|----------|------|------|----------|-------|------|----------|-------|--------|----------|
| Interval Start | | Eastboun | | V | Vestbour | ıd | N | orthbour | nd | S | outhbou | nd | Total | One Hour |
| Start | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT | 700 | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |



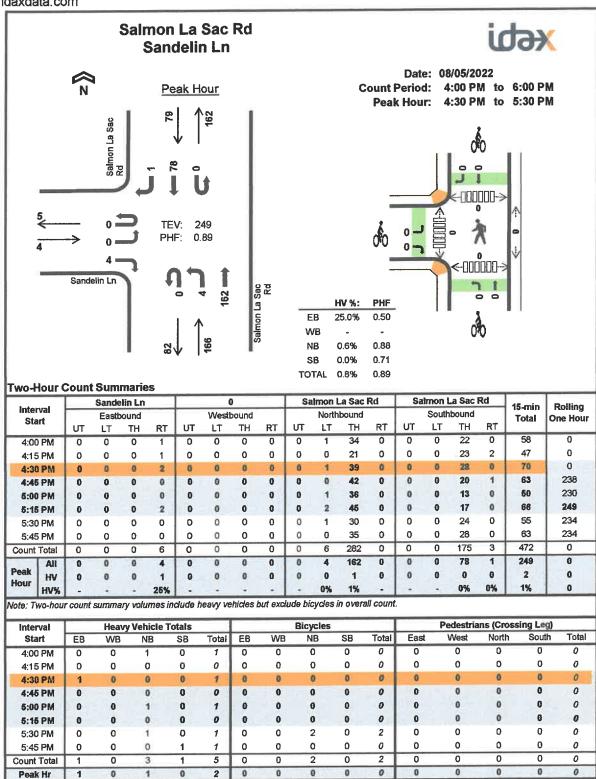
| | | - | 0 | | W | odswo | orth Lo | op | Sa | lmon i | .a Sac | Rd | Sa | ilmon L | a Sac | Rd | 15-min | Rolling |
|-------------------|----|------|-------|----|----|-------|---------|----|----|--------|--------|----|----|---------|-------|----|--------|----------|
| Interval Start | | East | oound | | | West | bound | | | North | bound | | | South | bound | | Total | One Hour |
| Start | UT | ŁT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 6:16 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 3 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | -1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |

| | | 0 | | Woo | sworth i | Loop | Salm | on La S | ac Rd | Salm | on La S | ac Rd | 15-min | Rolling |
|-------------------|----|---------|----|-----|----------|------|------|----------|-------|------|----------|-------|--------|----------|
| Interval Start | E | astboun | d | V | Vestbour | nd | 1 | lorthbou | nd | s | outhbour | nd | Total | One Hour |
| Oldit | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | . 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 |
| 5:45 PM | О | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |



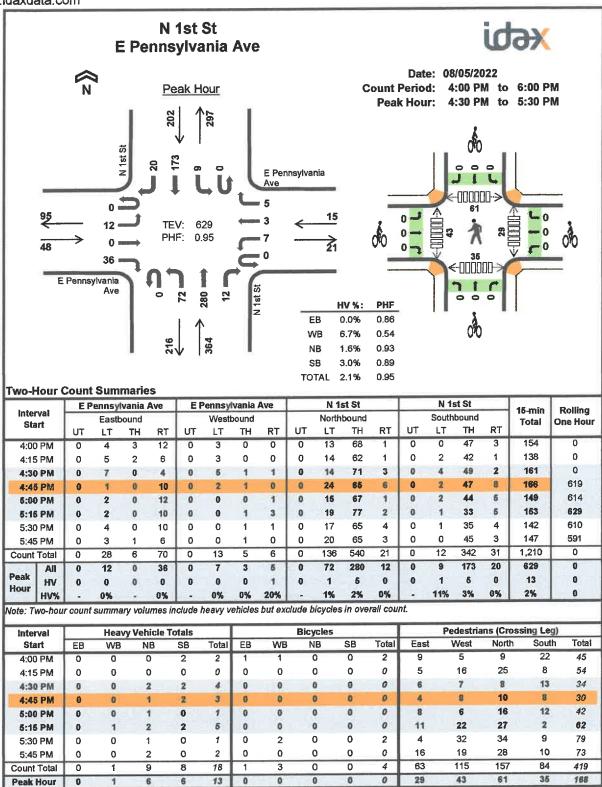
| | | 1 | D | | | Crav | vford | | Sa | lmon I | .a Sac | Rd | Sa | lmon L | a Sac | Rd | 15-min | Rolling |
|-------------------|----|-------|-------|----|----|------|-------|----|----|--------|--------|----|----|--------|-------|----|--------|----------|
| Interval Start | | Eastt | oound | | | West | bound | | | North | bound | | | South | bound | | Total | One Hour |
| Start | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | L.T | TH | RT | | One nous |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 1 |
| 6:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 3 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |

| | | 0 | | | Crawford | d | Salm | ion La S | ac Rd | Salm | on La Sa | ic Rd | 15-min | Rolling |
|-------------------|-----|----------|----|----|----------|----|------|----------|-------|------|----------|-------|--------|----------|
| Interval Start | - 1 | Eastboun | d | V | Vestbour | d | 1 | lorthbou | nd | s | outhbour | ıd | Total | One Hour |
| Start | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 |



| | | Sande | elin Ln | | | | 0 | | Sa | lmon i | .a Sac | Rd | Sa | lmon l | _a Sac | Rd | 16-min | Rolling |
|-------------------|----|-------|---------|-----|----|------|-------|----|----|--------|--------|----|----|--------|--------|----|--------|----------|
| Interval Start | | Eastl | oound | | | West | bound | | | North | bound | | | South | bound | | Total | One Hour |
| Start | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 11 | 2 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 3 |
| Count Total | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 1 | 0 | 5 | 0 |
| Peak Hour | 0 | 0 | 0 | - 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |

| | S | andelin L | _n | | 0 | | Salm | ion La S | ac Rd | Salm | on La Sa | ac Rd | 15-min | Rolling |
|-------------------|-----|-----------|----|----|----------|----|------|----------|-------|------|----------|-------|--------|----------|
| Interval Start | - 1 | astboun | d | V | Vestbour | nd | 1 | orthbou | nd | s | outhbour | nd | Total | One Hour |
| Start | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6:16 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |



| | EP | ennsy | lvania . | Ave | EP | ennsyl | lvania . | Ave | | N 1: | st St | | | N 1s | st St | | 16-min | Rolling |
|-------------------|----|-------|----------|-----|----|--------|----------|-----|----|-------|-------|----|----|-------|-------|----|--------|----------|
| Interval Start | | East | oound | | | West | bound | | | North | bound | | | South | bound | | Total | One Hour |
| Start | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | UT | LT | TH | RT | | |
| 4:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 2 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | - 4 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 0 | 3 | 9 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 8 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - 1 | 0 | 0 | 2 | 0 | 0 | -1 | - 1 | 0 | 5 | 13 |
| 5:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 10 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 9 |
| Count Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 8 | 0 | 0 | 1 | 6 | 1 | 18 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 6 | 0 | 0 | 1 | 5 | 0 | 13 | 0 |

| | E Per | nsylvan | ia Ave | E Pen | nsylvan | ia Ave | | N 1st \$1 | | | N 1st St | | 16-min | Rolling |
|-------------------|-------|----------|--------|-------|----------|--------|----|-----------|----|----|----------|----|--------|----------|
| Interval Start | | Eastboun | d | V | Vestbour | ıd | N | orthbour | nd | s | outhbour | nd | Total | One Hour |
| Start | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT | 1000 | One near |
| 4:00 PM | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 |
| 4:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:30 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 5:00 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:15 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5:30 PM | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 2 |
| 5:45 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Count Total | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 |
| Peak Hour | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Appendix B

LOS Result Worksheets

Existing 2022 Friday PM Peak Hour

| | | 4 | † | - | - | 1 |
|-------------------------|---|------|----------|------|------|------|
| | • | | | * | | _ |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | De la companya della companya della companya de la companya della | | 1 | | | 4 |
| Traffic Volume (vph) | 0 | 0 | 153 | 5 | 0 | 75 |
| Future Volume (vph) | 0 | 0 | 153 | 5 | 0 | 75 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | -1% | | 0% | | | 0% |
| Link Speed (mph) | 10 | | 35 | | | 35 |
| Link Distance (ft) | 423 | | 814 | | | 658 |
| Travel Time (s) | 28,8 | | 15.9 | | | 12.8 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 20% | 0% | 0% |
| Shared Lane Traffic (%) | | | | | | |
| Sign Control | Stop | | Free | | | Free |
| Intersection Summary | 1 715 45 | | - | | | |
| Area Type: | Other | | | | | -100 |

| | | 1 | † | - | 1 | 1 |
|-------------------------|-------|------|----------|------|------|------|
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 100 | | 1 | | | 4 |
| Traffic Volume (vph) | 1 | 2 | 155 | - 1 | 1 | 74 |
| Future Volume (vph) | 1 | 2 | 155 | 1 | 1 | 74 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | -2% | | 0% | | | -1% |
| Link Speed (mph) | 10 | | 35 | | | 35 |
| Link Distance (ft) | 415 | | 832 | | | 814 |
| Travel Time (s) | 28.3 | | 16.2 | | | 15.9 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (%) | 0% | 0% | 1% | 0% | 0% | 0% |
| Shared Lane Traffic (%) | | | | | | |
| Sign Control | Stop | | Free | | | Free |
| Intersection Summary | | | | | | |
| Area Type: | Other | | | | | 30 |

| Intersection | THE | | 110 | | | 3 10 |
|---|--------|--------|--------|--------|--------|-------|
| Int Delay, s/veh | 0 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | NO. | AATH | 13- | TABLE | DUL | 4 |
| | | 0 | 153 | 5 | 0 | 75 |
| Traffic Vol, veh/h | 0 | - | | | | |
| Future Vol, veh/h | 0 | 0 | 153 | 5 | 0 | 75 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | | | 0 | | - 100 | 0 |
| Grade, % | -1 | • | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 20 | 0 | 0 |
| Mymt Flow | 0 | 0 | 166 | 5 | 0 | 82 |
| MANUELION | | V. | 100 | | -360 | 1094 |
| | | | | | | |
| Major/Minor | Minor1 | | Major1 | - | Major2 | 100 |
| Conflicting Flow All | 251 | 169 | 0 | 0 | 171 | 0 |
| Stage 1 | 169 | 47 | - | | - | |
| Stage 2 | 82 | - | - | _ | _ | |
| Critical Hdwy | 6.2 | 6.1 | _ | | 4.1 | |
| Critical Hdwy Stg 1 | 5.2 | 0.1 | - | _ | Test. | |
| | 5.2 | | - | - | 100 | |
| Critical Hdwy Stg 2 | | | | | | |
| Follow-up Hdwy | 3.5 | 3.3 | - | | 2.2 | • |
| Pot Cap-1 Maneuver | 752 | 884 | | 0.5 | 1418 | 27.5 |
| Stage 1 | 874 | - | - | - | - | - |
| Stage 2 | 951 | - | | - | - | - |
| Platoon blocked, % | | | - | - | | - |
| Mov Cap-1 Maneuver | 752 | 884 | - | - | 1418 | |
| Mov Cap-2 Maneuver | 752 | - | - | - | - | - |
| Stage 1 | 874 | 7 4 | | | | |
| Stage 2 | 951 | _ | | | - | _ |
| Olage 2 | 301 | | = 0.7 | | | |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 0 | | 0 | | 0 | |
| HCM LOS | Α | | | | | |
| TOM LOO | | 200 | | | | 11 -8 |
| F | | 100000 | in n | almi i | e mi | a me |
| Minor Lane/Major Mvmt | | NBT | NBR | NBLn1 | SBL | SBT |
| Capacity (veh/h) | | | | | 1418 | |
| HCM Lane V/C Ratio | | - | - | - | - | - |
| HCM Control Delay (s) | | | * | 0 | 0 | - |
| HCM Lane LOS | | - | - | Α | Α | - |
| HCM 95th %tile Q(veh) | | | | | 0 | - |
| TOTAL OOD TODAY OF THE OUT OUT OF THE OUT OF THE OUT OF THE OUT OUT OF THE OUT OF THE OUT | | | | | | 2411 |

| Intersection | - 71 | 1971 | | .3.4 | 15 4 | |
|---------------------------|------------|----------|---|--------|----------|------------|
| Int Delay, s/veh | 0.2 | | | | | |
| | | 14000 | KIPST | KIPIPI | phi | COT |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 14s | | \$ | | | र्भ |
| Traffic Vol, veh/h | _ 1 | 2 | 155 | - 1 | - 1 | 74 |
| Future Vol, veh/h | 1 | 2 | 155 | 1 | 1 | 74 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | ٠ | None | - | None |
| Storage Length | 0 | - | - | - | | - |
| Veh in Median Storage, 1 | # 0 | | 0 | - | | 0 |
| Grade, % | -2 | - | 0 | - | - | -1 |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, % | 0 | 0 | 1 | 0 | 0 | 0 |
| Mymt Flow | 1 | 2 | 167 | 1 | 1 | 80 |
| Manual LIOM | T. | 6 | T.W.C | | - | 00 |
| | | | | | | |
| Major/Minor | Minor1 | | Major1 | | Major2 | 0.00 |
| Conflicting Flow All | 250 | 168 | 0 | 0 | 168 | 0 |
| Stage 1 | 168 | | N N IW | | | 100 |
| Stage 2 | 82 | - | - | - | _ | - |
| Critical Howy | 6 | 6 | | _ | 4.1 | - |
| Critical Howy Stg 1 | 5 | | | | 7.1 | |
| | 5 | - | | | | |
| Critical Hdwy Stg 2 | | | (#1 | _ | | |
| Follow-up Hdwy | 3.5 | 3.3 | - | - | 2.2 | - |
| Pot Cap-1 Maneuver | 764 | 890 | - | - | 1422 | - |
| Stage 1 | 883 | - | - | - | - | - |
| Stage 2 | 955 | | | | | - |
| Platoon blocked, % | | | - | - | | - |
| Mov Cap-1 Maneuver | 763 | 890 | - 20 | - 4 | 1422 | 160 |
| Mov Cap-2 Maneuver | 763 | - | | - | | - |
| Stage 1 | 883 | | | | | L, |
| | 954 | _ | - 30 | | | |
| Stage 2 | 304 | | • | | | _ |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 9,3 | | 0 | | 0.1 | |
| HCM LOS | A | | | | | |
| TOTAL EGG | - 14 | | | | | - |
| | | | 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | - Tarley | The sector |
| Minor Lane/Major Mymt | | NBT | NBR | WBLn1 | SBL | SBT |
| Capacity (veh/h) | 1 | | | 843 | 1422 | 1 1200 |
| HCM Lane V/C Ratio | | - | - | 0.004 | 0.001 | _ |
| HCM Control Delay (s) | | - 16 | 20 | 9.3 | 7.5 | 0 |
| HCM Lane LOS | | | | A | A | Α |
| HCM 95th %tile Q(veh) | 12 1 | Telleton | E. 25 | 0 | 0 | - 11 |
| LICINI 2081 JUNE (MIAGIL) | | 165 | - 50 | 0 | | 251 |

| | | A | † | - | - | 1 | |
|-------------------------|-------|----------|----------|--------|------|------|--|
| | (Alm) | VALIDITY | AMST | MODE | ODI | ODT | |
| Lane Group | WBL | WER | MBI | MBR | SBL | SBT | |
| Lane Configurations | N. | | To | | | 4 | |
| Traffic Volume (vph) | 1 | 0 | 157 | 6 | 0 | 80 | |
| Future Volume (vph) | 1 | 0 | 157 | 6 | 0 | 80 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Grade (%) | 2% | | 2% | | | -1% | |
| Link Speed (mph) | 10 | | 35 | | | 35 | |
| Link Distance (ft) | 589 | | 922 | | | 832 | |
| Travel Time (s) | 40.2 | | 18.0 | | | 16.2 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Heavy Vehicles (%) | 0% | 0% | 1% | 0% | 0% | 0% | |
| Shared Lane Traffic (%) | | | | | | | |
| Sign Control | Stop | | Free | | | Free | |
| Intersection Summary | , P | 300 | | | | | |
| Area Type: | Other | | Sin E | THE ST | | | |

| Intersection | | to Kill | 3418- | 3/11 | | |
|--------------------------|------------|-----------|--------------|-------|---------|---------|
| Int Delay, s/veh | 0 | | | | | |
| | WBL | WBR | NBT | NBR | SBL | SBT |
| Movement | | WEST | | PADIS | OUL | 4 |
| Lane Configurations | sh | | 1+ | | | 80 |
| Traffic Vol, veh/h | 1 | 0 | 157 | 6 | 0 | |
| Future Vol, veh/h | 1 | 0 | 157 | 6 | 0 | 80 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | | None | - 7 | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | - 4 | 0 | | | 0 |
| Grade, % | 2 | - | 2 | - | - | -1 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 0 | 0 | 1 | 0 | 0 | 0 |
| Mymt Flow | - 1 | 0 | 174 | 7 | 0 | 89 |
| | | | | | | |
| | F 40 1 1 1 | | A A C TO C W | | DECK OF | |
| | Minort | | Major1 | | Major2 | |
| Conflicting Flow All | 267 | 178 | 0 | 0 | 181 | 0 |
| Stage 1 | 178 | | - | . 2 | | - |
| Stage 2 | 89 | - | - | - | - | - |
| Critical Howy | 6.8 | 6,4 | - | - | 4.1 | - |
| Critical Hdwy Stg 1 | 5.8 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.8 | 14 | - | 10.00 | | |
| Follow-up Hdwy | 3.5 | 3.3 | _ | - | 2.2 | - |
| Pot Cap-1 Maneuver | 705 | 862 | E | 17/4 | 1407 | 11117 |
| Stage 1 | 841 | - | - | | - | - |
| Stage 2 | 930 | | - | | - 5 - | |
| Platoon blocked, % | 000 | | | | | _ |
| | 705 | 862 | | | 1407 | |
| Mov Cap-1 Maneuver | | | | | | |
| Mov Cap-2 Maneuver | 705 | | - | _ | | SHIII S |
| Stage 1 | 841 | 14 | | | - | |
| Stage 2 | 930 | - | - | | | |
| | | | | | | |
| Approach | -WB | | N8 | | SB | |
| HCM Control Delay, s | 10.1 | li de mes | 0 | 10 m | 0 | 10.0 |
| HCM LOS | В | | 0 | | 0 | |
| HCM LUS | В | | | | | |
| | 115-14 | | | | | |
| Minor Lane/Major Mymt | | NBT | NBR | WBLn1 | SBL | SBT |
| Capacity (veh/h) | il ein | 1 | | 705 | 1407 | |
| HCM Lane V/C Ratio | | - | _ | 0.002 | - | _ |
| HCM Control Delay (s) | | | | 10.1 | 0 | |
| HCM Lane LOS | | - | | В | A | - |
| HCM 95th %tile Q(veh) | | T-4 | | 0 | 0 | |
| HOW Sour While Clivery | | - | | 0 | - 0 | - |
| | | | | | | |

| Lane Group | | | - | | | | |
|-------------------------|------|--|------|------|------|------|--|
| TRUC DIOUP | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | 14 | | | 4 | 78 | | |
| Traffic Volume (vph) | 0 | 4 | 4 | 162 | 78 | 1 | |
| Future Volume (vph) | 0 | 4 | 4 | 162 | 78 | 1 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Grade (%) | 4% | and the state of t | | 2% | -2% | | |
| Link Speed (mph) | 35 | | | 10 | 10 | | |
| Link Distance (ft) | 159 | | | 549 | 922 | | |
| Travel Time (s) | 3.1 | | | 37.4 | 62.9 | | |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | |
| Heavy Vehicles (%) | 0% | 25% | 0% | 1% | 0% | 0% | |
| Shared Lane Traffic (%) | | | | | | | |
| Sign Control | Stop | | | Free | Free | | |

| Int Delay, s/veh 0.3 |
|--|
| Int Delay, s/veh Configurations Con |
| Lane Configurations |
| Lane Configurations Traffic Vol, veh/h Traffic Vol, veh/h O 4 4 4 162 78 1 Future Vol, veh/h O 0 0 0 0 0 0 0 0 0 0 0 0 |
| Traffic Vol, veh/h 0 4 4 162 78 1 Future Vol, veh/h 0 4 4 162 78 1 Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Stop Stop Free Free Free Free Free Free Free Free Free Ree Free |
| Future Vol, veh/h 0 4 4 162 78 1 Conflicting Peds, #/hr 0 0 0 0 0 0 Sign Control Stop Stop Free Free Free Free RT Channelized - None - None - None Storage Length 0 0 0 Grade, % 4 2 2 -2 - Peak Hour Factor 89 89 89 89 89 89 89 89 89 89 89 89 89 |
| Conflicting Peds, #hr 0 |
| Sign Control Stop Stop Free Abone Conflicting Flow All 279 89 89 0 - 0 Stage 1 89 - - - -< |
| RT Channelized |
| Storage Length 0 - |
| Veh in Median Storage, # 0 - - 0 0 Grade, % 4 - - 2 -2 - Peak Hour Factor 89 89 89 89 89 89 89 89 89 89 89 89 89 89 89 1 0 0 Milor White Institute Insti |
| Veh in Median Storage, # 0 - - 0 0 Grade, % 4 - - 2 -2 - Peak Hour Factor 89 89 89 89 89 89 89 89 89 89 89 89 89 89 89 1 0 |
| Grade, % 4 2 -2 - Peak Hour Factor 89 89 89 89 89 89 Heavy Vehicles, % 0 25 0 1 0 0 Mwmt Flow 0 4 4 182 88 1 Major/Minor Minor2 Major 2 Conflicting Flow All 279 89 89 0 - 0 Stage 1 89 Stage 2 190 |
| Heavy Vehicles, % 0 25 0 1 0 0 Mvmt Flow 0 4 4 182 88 1 Major Minor Minor Major Major C Conflicting Flow All 279 89 89 0 - 0 Stage 1 89 Stage 2 190 |
| Mynt Flow 0 4 4 182 88 1 Major Minor Minor Major 2 |
| Mymt Flow 0 4 4 182 88 1 Major Minor Minor Major Mijor Major 2 Major 2 Conflicting Flow All 279 89 89 0 - 0 Stage 1 89 - - - - - - Stage 2 190 - - - - - - |
| Conflicting Flow All 279 89 89 0 - 0 Stage 1 89 - - - - - - Stage 2 190 - - - - - - |
| Conflicting Flow All 279 89 89 0 - 0 Stage 1 89 |
| Conflicting Flow All 279 89 89 0 - 0 Stage 1 89 - - - - - - Stage 2 190 - - - - - - |
| Stage 1 89 |
| Stage 2 190 |
| |
| College Udgas 7.2 6.95 4.4 |
| |
| Critical Howy Stg 1 6.2 |
| Critical Hdwy Stg 2 6.2 |
| Follow-up Hdwy 3.5 3.525 2.2 |
| Pot Cap-1 Maneuver 672 900 1519 |
| Stage 1 921 |
| Stage 2 812 |
| Platoon blocked, % |
| Mov Cap-1 Maneuver 670 900 1519 |
| Mov Cap-2 Maneuver 670 |
| Stage 1 918 |
| Stage 2 812 |
| Stage 2 612 |
| STATE AND INSCREPANCE OF MICH. |
| Approach EB NB SE |
| HCM Control Delay, s 9 0.2 0 |
| HCM LOS A |
| |
| Minor Lane/Major Mymt NBL NBT EBLn1 SBT SBR |
| |
| Capacity (veh/h) 1519 - 900 |
| HCM Lane V/C Ratio 0.003 - 0.005 |
| HCM Control Delay (s) 7.4 0 9 |
| HCM Lane LOS A A A |
| HCM 95th %tile Q(veh) 0 - 0 |

Lanes, Volumes, Timings 5: S 1st St/N 1st St & W Pennsylvania Ave/E Pennsylvania Ave

| | 1 | → | ~ | 1 | 4 | 4 | 4 | 1 | 1 | - | ↓ | 1 |
|-------------------------|-------|----------|------|------|------|------|------|------|------|------|----------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WSR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | | | | do | |
| Traffic Volume (vph) | 12 | 0 | 36 | 7 | 3 | 5 | 72 | 280 | 12 | 9 | 173 | 20 |
| Future Volume (vph) | 12 | 0 | 36 | 7 | 3 | 5 | 72 | 280 | 12 | 9 | 173 | 20 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | | 0% | | | 0% | | | 5% | | | -2% | |
| Link Speed (mph) | | 25 | | | 25 | | | 25 | | | 25 | |
| Link Distance (ft) | | 330 | | | 456 | | | 339 | | | 344 | |
| Travel Time (s) | | 9.0 | | | 12.4 | | | 9.2 | | | 9.4 | |
| Confl. Peds. (#/hr) | 61 | | 35 | 35 | | 61 | 43 | | 29 | 29 | | 43 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 0% | 20% | 1% | 2% | 0% | 11% | 3% | 0% |
| Parking (#/hr) | 0 | 0 | 0 | - 0 | 0 | 0 | | | | | | |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |

| Int Delay, s/veh | 2.4 | | | | | | | | | | | |
|-------------------------------|---------|------|---------|--------|--------|--------|----------|----------|----------|-----------|-------|--------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5+57L | 440 | 845015 | 44.000 | d) | 11011 | 3 13,000 | 44. | | - | 4 | |
| Traffic Vol., veh/h | 12 | 0 | 36 | 7 | 3 | 5 | 72 | 280 | 12 | 9 | 173 | 20 |
| Future Vol, veh/h | 12 | 0 | 36 | 7 | 3 | 5 | 72 | 280 | 12 | 9 | 173 | 20 |
| | 61 | 0 | 35 | 35 | 0 | 61 | 43 | 0 | 29 | 29 | 0 | 43 |
| Conflicting Peds, #/hr | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| Sign Control | | | None | Stop | Slup | None | 1166 | 1166 | None | 1100 | 1100 | None |
| RT Channelized | 1 | | None | 9100 | | TAINLE | | ALII S | Nunc | - 11200 | , _ | INUITO |
| Storage Length | - | - 0 | | | 0 | - | | 0 | | No. | 0 | A - A- |
| Veh in Median Storage, | | 0 | - | V 115 | 0 | | | 5 | | | -2 | _ |
| Grade, % | ne | 0 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Peak Hour Factor | 95 | 95 | | 0.0 | 95 | 20.00 | 95 | 2 | 90 | 11 | 3 | 0 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 3 | 20 | 76 | 295 | 13 | 9 | 182 | 21 |
| Mymt Flow | 13 | 0 | 38 | | 3 | 0 | (0) | 590 | 13 | 3 | 102 | - 21 |
| Major/Minor | Minor2 | | 10.57 | Minort | | = 11 | Majort | 100 | , L | Major2 | | |
| Conflicting Flow All | 773 | 743 | 271 | 748 | 747 | 392 | 246 | 0 | 0 | 337 | 0 | 0 |
| Stage 1 | 254 | 254 | 211 | 483 | 483 | TES PO | 210 | | TI O RES | 155 | UT US | |
| Stage 2 | 519 | 489 | _ | 265 | 264 | _ | _ | _ | | + | - | _ |
| Critical Hdwy | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.4 | 4.11 | 100 | - | 4.21 | | DES. |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | 0.2 | 6.1 | 5.5 | 0,4 | 7,17 | | - | - | _ | |
| Critical Howy Stg 2 | 6,1 | 5.5 | May 1 | 6.1 | 5.5 | | a le | 3 | | - | | w 5 |
| Follow-up Hdwy | 3.5 | 4 | 3.3 | 3.5 | 4 | 3,48 | 2.209 | | - | 2.299 | - | _ |
| Pot Cap-1 Maneuver | 319 | 346 | 773 | 331 | 344 | 619 | 1326 | | | 1174 | | 1,000 |
| Stage 1 | 755 | 701 | 110 | 569 | 556 | 010 | 1020 | | | | - | - |
| Stage 2 | 544 | 553 | | 745 | 694 | | | | | | -100 | |
| Platoon blocked, % | Jana | 000 | | TTU | PUT | | | | - | | | |
| Mov Cap-1 Maneuver | 266 | 297 | 717 | 277 | 295 | 567 | 1272 | STATE OF | н | 1142 | | 012 |
| | 266 | 297 | 111 | 277 | 295 | 307 | 1412 | | - | A. I. The | | - |
| Mov Cap-2 Maneuver Stage 1 | 672 | 666 | I V A | 513 | 502 | | No. | | | March 1 | | 110 |
| | 468 | 499 | | 676 | 659 | - | | | | _ | | |
| Stage 2 | 400 | 433 | | 010 | 003 | | w j | 1/8 | 9.5 | | ST. | TA HE |
| Approach | EB | | 811 | WB | | 95.1 | NB | 11,5 | 99 | SB | | TO L |
| HCM Control Delay, s | 12.9 | | NATE OF | 16.1 | ERE | | 1.6 | | | 0.4 | Cont | |
| HCM LOS | В | | | C | | | 110 | | | | | |
| I IOIN LOG | ن ا | | | | | | | | | | | |
| Minor Lane/Major Mvmt | | NB). | NBT_ | NBR | EBLn1/ | | SBL | SET | SBR | | | 5,80 |
| Capacity (veh/h) | 1 30 52 | 1272 | | | 504 | 339 | 1142 | | 1241 | | | |
| HCM Lane V/C Ratio | | 0.06 | - | | 0.1 | 0.047 | 0.008 | _ | _ | | | |
| HCM Control Delay (s) | | 8 | 0 | 1181 | 12.9 | 16.1 | 8.2 | 0 | - | | | |
| HCM Lane LOS | | Α | Α | - | В | C | Α | Α | | | | |
| HCM 95th %tile Q(veh) | | 0.2 | -7 | | 0.3 | 0.1 | 0 | | | | | |

2023 No Action PM Peak Hour

| | 6 | 4 | † | 1 | - | ļ | |
|-------------------------|-------|------|----------|------|------|------|-------------------------------------|
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT | prik suite die 181 dae de 181 de 18 |
| Lane Configurations | NyF | | 40. | | | 4 | |
| Traffic Volume (vph) | 0 | 0 | 156 | 5 | 0 | 77 | |
| Future Volume (vph) | 0 | 0 | 156 | 5 | 0 | 77 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Grade (%) | -1% | | 0% | | | 0% | |
| Link Speed (mph) | 10 | | 35 | | | 35 | |
| Link Distance (ft) | 423 | | 814 | | | 658 | |
| Travel Time (s) | 28.8 | | 15.9 | | | 12.8 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Heavy Vehicles (%) | 0% | 0% | 0% | 20% | 0% | 0% | |
| Shared Lane Traffic (%) | | | | | | | |
| Sign Control | Stop | | Free | | | Free | |
| Intersection Summary | | | | | | | |
| Area Type: | Other | | | | | | |

| Intersection | | | | | | |
|---|--------|-------|---------|-----------|---------|----------|
| Int Delay, s/veh | 0 | | | | | |
| Movement | WBL | WBR | NBT | NER | SBL | SBT |
| | | ARTON | _ | Other | DUL | |
| Lane Configurations | W | 0 | 100 | | 0 | 4 |
| Traffic Vol., veh/h | 0 | 0 | 156 | 5 | 0 | 77 |
| Future Vol, veh/h | 0 | 0 | 156 | 5 | 0 | 77 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | | None | | None | | None |
| Storage Length | 0 | .*: | - | | - | - |
| Veh in Median Storage, # | 0 | 1 | 0 | | BUN | 0 |
| Grade, % | -1 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 0 | 0 | 0 | 20 | 0 | 0 |
| Mymt Flow | 0 | 0 | 170 | 5 | 0 | 84 |
| MAUNT LIOM | U | 0 | 110 | 9 | U | 04 |
| | | | | | | |
| Major/Minor | Minori | | Majori | | Major2 | |
| Conflicting Flow All | 257 | 173 | 0 | 0 | 175 | 0 |
| Stage 1 | 173 | 1- | A. 14 | - 10. | | - |
| Stage 2 | 84 | _ | | - | | - |
| Critical Hdwy | 6.2 | 6.1 | 112 | | 4.1 | |
| | 5.2 | 46.1 | | | 74.1 | _ |
| Critical Hdwy Stg 1 | 5.2 | | | | | SALEU EL |
| Critical Hdwy Stg 2 | | | | 127.50 | | |
| Follow-up Hdwy | 3.5 | 3.3 | | - | 2.2 | - |
| Pot Cap-1 Maneuver | 747 | 880 | - | | 1414 | - |
| Stage 1 | 870 | - | - | | - | - |
| Stage 2 | 949 | - 3 | | | 1 | |
| Platoon blocked, % | | | - | - | | - |
| Mov Cap-1 Maneuver | 747 | 880 | | | 1414 | |
| Mov Cap-2 Maneuver | 747 | - | - | - | - | - |
| Stage 1 | 870 | | | 101 2 | 1743 | - |
| Stage 2 | 949 | - | | _ | - | - |
| Clago L | - | | | | | |
| | | | - | | - | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 0 | | 0 | | 0 | |
| HCM LOS | Α | | | | | |
| | | | | | | |
| AND THE RESIDENCE OF THE PARTY | | AIRT | AUDIO 1 | union see | evitor. | CDT |
| Minor Lane/Major Mymt | _ | NBT | LARRE | WBLnt | SBL | SBT |
| Capacity (veh/h) | | 8 3 | - | | 1414 | |
| HCM Lane V/C Ratio | | - | - | - | - | - |
| HCM Control Delay (s) | | | | 0 | 0 | |
| HCM Lane LOS | | - | - | Α | Α | - |
| HCM 95th %tile Q(veh) | | | - | | 0 | |
| The same and said | | | | | | |

| | 6 | 1 | † | - | - | 1 | | |
|-------------------------|----------|---------|------------------|--------|------|------|-----------------|--|
| | | 11/2009 | Name of the last | 4.00 m | 0.00 | dive | | |
| Lane Group | MBT | WBR | NBT | NBR | SBL | SBT | | |
| Lane Configurations | A. | | 10 | | | 4 | | |
| Traffic Volume (vph) | ALC: NO. | 2 | 158 | - 1 | 1 | 75 | | |
| Future Volume (vph) | 1 | 2 | 158 | 1 | 1 | 75 | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | |
| Grade (%) | -2% | | 0% | | | -1% | | |
| Link Speed (mph) | 10 | | 35 | | | 35 | | |
| Link Distance (ft) | 415 | | 832 | | | 814 | | |
| Travel Time (s) | 28,3 | | 16.2 | | | 15.9 | | |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | | |
| Heavy Vehicles (%) | 0% | 0% | 1% | 0% | 0% | 0% | | |
| Shared Lane Traffic (%) | | | | | | | | |
| Sign Control | Stop | | Free | | | Free | | |
| | | | | | | | | |
| Intersection Summary | | | | | | | and the same of | |
| Area Type: | Other | | | | | | | |

| Intersection | | | 3 - | | | |
|---|-----------|----------|--------------|-------|---------|--------|
| Int Delay, s/veh | 0.1 | | | | | |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | M | | 1 | | | d |
| Traffic Vol, veh/h | 1 | 2 | 158 | 1 | 1 | 75 |
| Future Vol, veh/h | 1 | 2 | 158 | 1 | 1 | 75 |
| Conflicting Peds, #/hr | 0 | 0 | - 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | Algo- | None | - | None | | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | | 0 | 5 | - | 0 |
| Grade, % | -2 | | 0 | - | 2 | -1 |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, % | 0 | 0 | 1 | 0 | 0 | 0 |
| Mymt Flow | 1 | 2 | 170 | 1 | 14 | 81 |
| | | | | | | |
| NAME OF TAXABLE PARTY. | P. Const. | | 6 th colored | _ | Name of | _ |
| Color CAMPAGIA | Minor1 | | Major1 | | Major2 | _ |
| Conflicting Flow All | 254 | 171 | 0 | 0 | 171 | 0 |
| Stage 1 | 171 | 100 | 100 | | | |
| Stage 2 | 83 | - | | _ | | - |
| Critical Hdwy | 6 | 6 | * | | 4.1 | |
| Critical Hdwy Stg 1 | 5 | - | - | _ | - | |
| Critical Hdwy Stg 2 | 5 | - | | | | |
| Follow-up Hdwy | 3.5 | 3.3 | | | 2.2 | - |
| Pot Cap-1 Maneuver | 760 | 886 | - 1 | - | 1418 | - |
| Stage 1 | 880 | - | - | - | - | - |
| Stage 2 | 954 | 16 | | - 4 | | - Tet. |
| Platoon blocked, % | | | - | - | | - |
| Mov Cap-1 Maneuver | 759 | 886 | - | 27 | 1418 | |
| Mov Cap-2 Maneuver | 759 | | _ | - | - | - |
| Stage 1 | 880 | | | | 100 | 1 |
| Stage 2 | 953 | - | - | - | _ | - |
| | | | | | | |
| Branch and | LAVES | | NB | | SB | |
| Approach | WB | - | | | | - |
| HCM Control Delay, s | 9.3 | | 0 | | 0.1 | |
| HCM LOS | Α | | | | | |
| | | | | | | |
| Minor Lane/Major Mirnt | - | NBT | NBR | WBEn1 | SBL | SBT |
| Capacity (veh/h) | 100 | | - 11- | 839 | 1418 | |
| HCM Lane V/C Ratio | | - | - | 0.004 | 0,001 | |
| HCM Control Delay (s) | | | | 9.3 | 7.5 | 0 |
| HCM Lane LOS | | | _ | A | A | A |
| HCM 95th %tile Ci(veh) | | TOTAL ST | Martin V | 0 | 0 | IIR V |
| I IOM 2001 WING 20 ACM | | 100 | | V | U | 16 |

| | | 1 | † | - | 1 | 1 | |
|-------------------------|-------|------|----------|------|------|------|--|
| | • | | | • | | - | |
| Larie Group | WBL | WBR | NBT | MBR | SBL | SBT | |
| Lane Configurations | W | | 10 | | | 4 | |
| Traffic Volume (vph) | 1 | 0 | 160 | 6 | 0 | 82 | |
| Future Volume (vph) | 1 | 0 | 160 | 6 | 0 | 82 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Grade (%) | 2% | | 2% | | | -1% | |
| Link Speed (mph) | 10 | | 35 | | | 35 | |
| Link Distance (ft) | 589 | | 922 | | | 832 | |
| Travel Time (s) | 40.2 | | 18.0 | | | 16,2 | |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | |
| Heavy Vehicles (%) | 0% | 0% | 1% | 0% | 0% | 0% | |
| Shared Lane Traffic (%) | | | | | | | |
| Sign Control | Stop | | Free | | | Free | |
| | | - | | - | | 1 | |
| Intersection Summary | Other | | | | | 8880 | |
| Area Type: | Other | | | | | | |

| Intersection | 13/ | | | V. U.S. | | |
|--------------------------|----------|--------|---------|-----------|---------|--------------|
| Int Delay, s/veh | 0 | | | | | |
| | WBL | WBR | NBT | NBR | SBL | SBT |
| Movement | | WARK | | PARTIE | 900 | |
| Lane Configurations | W | | 100 | | | 4 |
| Traffic Vol, veh/h | 1 | 0 | 160 | 6 | 0 | 82 |
| Future Vol, veh/h | 1 | 0 | 160 | 6 | 0 | 82 |
| Conflicting Peds, #fhr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | 45. | None | | None | | None |
| Storage Length | 0 | - | - | - | - | _ |
| Veh in Median Storage, # | | - | 0 | | 1 | 0 |
| Grade, % | 2 | - | 2 | - | - | -1 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 0 | 0 | 1 | 0 | 0 | 0 |
| Mymt Flow | 1 | 0 | 178 | 7 | 0 | 91 |
| | | | 1111.51 | | | |
| | | | | | | |
| | Mirror 1 | | Major1 | | Major2 | |
| Conflicting Flow All | 273 | 182 | 0 | 0 | 185 | 0 |
| Stage 1 | 182 | 0.34 | | | 0.00 | |
| Stage 2 | 91 | - | - | - | - | - |
| Critical Howy | 6,8 | 6.4 | | - 2 | 4,1 | |
| Critical Hdwy Stg 1 | 5.8 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.8 | | - | | - 10 | - |
| Follow-up Hdwy | 3.5 | 3.3 | - | - | 2.2 | - |
| Pot Cap-1 Maneuver | 699 | 857 | 10/45 | | 1402 | |
| Stage 1 | 837 | _ | - | | - | - |
| Stage 2 | 928 | 9.0.0 | - 1 2 | | - 200 | UKI . |
| Platoon blocked, % | | | _ | | | _ |
| Mov Cap-1 Maneuver | 699 | 857 | | | 1402 | 1 |
| Mov Cap-2 Maneuver | 699 | 001 | | | 1710/6 | |
| | 837 | | | | | No. |
| Stage 1 | | | | | A = 07. | - |
| Stage 2 | 928 | | - | - | | E PROVINCE V |
| | | | | | | |
| Approach | WB | | NB | | SB | |
| HCM Control Delay, s | 10.2 | STORY | 0 | | 0 | |
| HCM LOS | В | | | | | |
| | | | 3 1 1 | | | |
| | | 133000 | a share | Water Con | W.D.I | 0.07 |
| Minor Lane/Major Mvmt. | | NBT | NBR | WBLn1 | SBL | SBT |
| Capacity (veh/h) | | | | 699 | 1402 | 1 35 |
| HCM Lane V/C Ratio | | - | | 0.002 | - | - |
| HCM Control Delay (s) | | | | 10.2 | 0 | 14 |
| HCM Lane LOS | | - | - | В | Α | - |
| HCM 95th %tile Q(veh) | | - | | 0 | 0 | |
| | | | | | | |

| | * | ~ | 4 | + | 1 | 4 | | |
|-------------------------|----------|------|------|----------|------|------|---|-----|
| | _ | • | ` | | _ | | | |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | | |
| Lane Configurations | MA | | | 4 | 1 | | | |
| Traffic Volume (vph) | 0 | 4 | -4 | 165 | 80 | 1 | | |
| Future Volume (vph) | 0 | 4 | 4 | 165 | 80 | 1 | | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | | |
| Grade (%) | 4% | | | 2% | -2% | | | |
| Link Speed (mph) | 35 | | | 10 | 10 | | | |
| Link Distance (ft) | 159 | | | 549 | 922 | | | |
| Travel Time (s) | 3.1 | | | 37.4 | 62.9 | | | |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | | |
| Heavy Vehicles (%) | 0% | 25% | 0% | 1% | 0% | 0% | | |
| Shared Lane Traffic (%) | | | | | | | | |
| Sign Control | Stop | | | Free | Free | | | |
| | | | | | | | - | 7.5 |
| Intersection Summary | 200 | | | | | | | |
| Area Type: | Other | | | | | | | |

| | - | | | | | |
|---------------------------------------|--------|---------------|----------|--------|---------|---------|
| Intersection | | | | 911 | | |
| Int Delay, s/veh | 0.3 | | | | | |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | N. S. | - September 1 | 7100 | र्व | 7. | 2000 |
| Traffic Vol., veh/h | 0 | 4 | 4 | 165 | 80 | - 1 |
| Future Vol, veh/h | 0 | 4 | 4 | 165 | 80 | 1 |
| Conflicting Peds, #/hr | 0 | 0 | - 0 | 100 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | GIOD | None | 1100 | | 1100 | None |
| Storage Length | 0 | 110116 | | 140110 | - | 140HO |
| Veh in Median Storage, # | | TURE | | 0 | 0 | |
| Grade, % | 4 | 10= 7E | - | 2 | -2 | |
| | 89 | 89 | 89 | 89 | 89 | 89 |
| Peak Hour Factor | 09 | 25 | 09 | 1 | 0 | 0 |
| Heavy Vehicles, % | | 4 | 4 | | 90 | 1 |
| Nomt Flow | 0 | 4 | 4 | 185 | 90 | 1. |
| | | | | | | |
| Major/Minor / | Minor2 | البجا | Majort . | | Major2 | |
| Conflicting Flow All | 284 | 91 | 91 | 0 | - | 0 |
| Stage 1 | 91 | - | -1 | | 1 - 4 | |
| Stage 2 | 193 | | - | - | - | |
| Critical Hdwy | 7.2 | 6.85 | 4.1 | | 18 | - |
| Critical Hdwy Stg 1 | 6.2 | - | - | | - | - |
| Critical Hdwy Stg 2 | 6,2 | - A TW. | 100 | 5 | | |
| Follow-up Hdwy | 3.5 | 3.525 | 2.2 | | | - |
| Pot Cap-1 Maneuver | 667 | 898 | 1517 | | | - |
| Stage 1 | 919 | - | 0.500 | | - | |
| Stage 2 | 809 | 200 | | | 101 | HMI. |
| Platoon blocked, % | -000 | | | | - | - |
| Mov Cap-1 Maneuver | 665 | 898 | 1517 | | | 12 2 |
| Mov Cap-1 Maneuver | 665 | 000 | 1011 | | | _ |
| Stage 1 | 916 | EWIE H | | | 111.552 | - |
| | 809 | | 11.50 | | | |
| Stage 2 | 009 | | | | Meses W | |
| | | | | | | |
| Approach | EB | | NB. | | SB | |
| HCM Control Delay, s | 9 | | 0.2 | | 0 | |
| HCM LOS | Α | | | | | |
| | | | | | | |
| DESCRIPTION OF STREET | | NBL | 8.85VF | EBLn1 | SBT | SER |
| Minor Lane/Major Mymt | | | | | | SOF |
| Capacity (veh/h) | | 1517 | - 100 | 898 | | 11/12/2 |
| HCM Lane V/C Ratio | | 0.003 | | | - | _ |
| HCM Control Delay (s) | | 7.4 | 0 | 9 | | |
| | | | 4 | | | |
| HCM Lane LOS HCM 95th %tile Q(veh) | | A | A | A | 40 | _ |

5: S 1st St/N 1st St & W Pennsylvania Ave/E Pennsylvania Ave

| | • | - | * | 1 | - | * | 4 | † | - | 1 | 1 | 1 |
|-------------------------|--------|------|-------|---------|------|------|------|----------|------|------|------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR. | SBL | SBT | SBR |
| Lane Configurations | | do. | | | 4 | | | 40 | | | 4 | |
| Traffic Volume (vph) | 12 | 0 | 37 | 7 | 3 | 5 | 73 | 286 | 12 | 9 | 176 | 20 |
| Future Volume (vph) | 12 | 0 | 37 | 7 | 3 | 5 | 73 | 286 | 12 | 9 | 176 | 20 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | | 0% | | | 0% | | | 5% | | | -2% | |
| Link Speed (mph) | | 25 | | | 25 | | | 25 | | | 25 | |
| Link Distance (ft) | | 330 | | | 456 | | | 339 | | | 344 | |
| Travel Time (s) | | 9.0 | | | 12.4 | | | 9.2 | | | 9.4 | |
| Confl. Peds. (#/hr) | 61 | | 35 | 35 | | 61 | 43 | | 29 | 29 | | 43 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 0% | 20% | 1% | 2% | 0% | 11% | 3% | 0% |
| Parking (#/hr) | 0 | - 0 | 0 | 0 | 0 | 0 | | | | | | |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Intersection Summary | 1, 111 | | N = 1 | es aris | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |

| Intersection | | | | | 310 | | | | | | | |
|--|--------|-------|----------------|------------|----------|-----------|-------------|--------|-------|--------|-------|-------|
| Int Delay, s/veh | 2.4 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | TEW | WER | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | e die | | | 4 | | | 4 | | | 4 | |
| Traffic Vol. yeh/h | 12 | 0 | 37 | 7 | 3 | 5 | 73 | 286 | 12 | 9 | 176 | 20 |
| Future Vol., veh/h | 12 | 0 | 37 | 7 | 3 | 5 | 73 | 286 | 12 | 9 | 176 | 20 |
| Conflicting Peds, #/hr | 61 | 0 | 35 | 35 | 0 | 61 | 43 | 0 | 29 | 29 | 0 | 43 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | | 2 1 | None | T VE | 100 | None | | - | None | - | | None |
| Storage Length | | - | - | - | 1.0 | - | - | - | - | - | - | - |
| Veh in Median Storage, | # - | 0 | 14 9 | 1 1 5 | 0 | 70,72 | IV I SX | 0 | - New | | 0 | - |
| Grade, % | - | 0 | - | - | 0 | - | - | 5 | | - | -2 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 20 | 1 | 2 | 0 | 11 | 3 | 0 |
| Mymt Flow | 13 | 0 | 39 | 7 | 3 | 5 | 77 | 301 | 13 | 9 | 185 | 21 |
| | | | | | | | | | | | | |
| Major/Minor | Minor2 | | | Minort | 7.10 | | Major 1 | | | Major2 | | |
| Conflicting Flow All | 784 | 754 | 274 | 759 | 758 | 398 | 249 | 0 | 0 | 343 | 0 | 0 |
| Stage 1 | 257 | 257 | | 491 | 491 | | B - | 4-31- | 1000 | 3 | | 100 |
| Stage 2 | 527 | 497 | - | 268 | 267 | - | - | - | - | - | - | |
| Critical Hdwy | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.4 | 4.11 | - | | 4.21 | | |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | | 6.1 | 5.5 | - | - | - | - | - | - | |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | - + | 6.1 | 5.5 | 17 | 100 | | | - | | |
| Follow-up Hdwy | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.48 | 2.209 | - | - | 2.299 | - | - |
| Pot Cap-1 Maneuver | 313 | 341 | 770 | 326 | 339 | 614 | 1323 | | 2 4 | 1167 | | - |
| Stage 1 | 752 | 699 | - | 563 | 552 | - | - | - | - | | - | - |
| Stage 2 | 538 | 548 | | 742 | 692 | | - 35 | 1 2 3 | | | - 1 | |
| Platoon blocked, % | | | | in as life | | 50000 | Contract of | - | - | | _ | - |
| Mov Cap-1 Maneuver | 260 | 292 | 714 | 272 | 290 | 562 | 1269 | 00 m | 200 | 1135 | | |
| Mov Cap-2 Maneuver | 260 | 292 | - | 272 | 290 | - | - | - | - | | - | - |
| Stage 1 | 668 | 664 | - : | 507 | 497 | | 1 | | | - | | |
| Stage 2 | 462 | 493 | - | 672 | 657 | | | THE CO | - | - | | - |
| | | | | | | | | | | | Ves V | 1011 |
| Approach | EB | | | WB | | | NB | | 0 111 | SB | | Heri. |
| HCM Control Delay, s | 13 | 1571 | I ESTATI | 16,3 | | | 1,6 | | | 0.4 | | |
| HCM LOS | В | | | С | | | | | | | | |
| Payte due la | | 2.751 | Name of Street | AMERICA | Pint - V | OLOPO WAY | (SPA) | ner. | opp | | | |
| Minor Lane/Major Mvmt | | NBL | NBT | NBR | EBLn1. | | SBL | SBT | SBR | | | |
| Capacity (veh/h) | | 1269 | | | 500 | 334 | 1135 | | 11.5 | | | |
| HCM Lane V/C Ratio | | 0.061 | - | | 0.103 | 0.047 | 0.008 | - 0 | - | | | |
| HCM Control Delay (s) | | 8 | 0 | | 13 | 16.3 | 8.2 | 0 | 1.00 | | | |
| HCM Lane LOS | | A | Α | - | В | C | Α | Α | _ | | | |
| HCM 95th %tile Q(veh) | | 0.2 | | | 0.3 | 0.1 | 0 | Desc. | - | | | |

Traffic Impact Analysis The Outpost at Lake Cle Elum – Kittitas County, WA

2023 With Project Friday PM Peak Hour

| | | 4 | † | - | - | 1 |
|-------------------------|-------|------|----------|------|------|------|
| | • | _ | _ ! | - / | | |
| Lane Group | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 14 | | To. | | | 4 |
| Traffic Volume (vph) | 0 | 0 | 158 | 5 | 0 | 80 |
| Future Volume (vph) | 0 | 0 | 158 | 5 | 0 | 80 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | -1% | | 0% | | | 0% |
| Link Speed (mph) | 10 | | 35 | | | 35 |
| Link Distance (ft) | 423 | | 814 | | | 658 |
| Travel Time (s) | 28,8 | | 15.9 | | | 12.8 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 20% | 0% | 0% |
| Shared Lane Traffic (%) | | | | | | |
| Sign Control | Stop | | Free | | | Free |
| Intersection Summary | | | | | | |
| Area Type: | Other | | | | 999 | |

| Intersection | | | | | | |
|------------------------|--------|---------|--------|---------------------------------------|--------|-----------|
| Int Delay, s/veh | 0 | | | | | |
| Movement | WELL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | W | and the | 1- | S S S S S S S S S S S S S S S S S S S | UNIT | 4 |
| Traffic Vol, veh/h | 0 | 0 | 158 | 5 | 0 | 80 |
| Future Vol. veh/h | 0 | 0 | 158 | 5 | 0 | 80 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | Stop | None | 1100 | None | 1100 | None |
| | 0 | NORE | | HOHE | | IADIR |
| Storage Length | _ | | 0 | 1 1 2 | - | 0 |
| Veh in Median Storage, | 0 | | | | | 0 |
| Grade, % | -1 | 55 | 0 | 00 | 02 | 92 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | |
| Heavy Vehicles, % | 0 | 0 | 0 | 20 | 0 | 0 |
| Mymt Flow | 0 | 0 | 172 | - 5 | 0 | 87 |
| | | | | | | |
| Major/Minor | Minort | | Majort | | Major2 | |
| Conflicting Flow All | 262 | 175 | 0 | 0 | 177 | 0 |
| | 175 | 110 | 0 | | 111 | |
| Stage 1 | 87 | | - | | | |
| Stage 2 | 6.2 | 6.1 | i i ia | | 4.1 | 4 |
| Critical Howy | | | | | | |
| Critical Hdwy Stg 1 | 5.2 | | - | | - | SUE IV |
| Critical Hdwy Stg 2 | 5.2 | 2.2 | | | 2.2 | |
| Follow-up Hdwy | 3.5 | 3.3 | | - | | _ |
| Pot Cap-1 Maneuver | 742 | 878 | | | 1411 | |
| Stage 1 | 869 | | - | - | _ | |
| Stage 2 | 946 | | | -5 | 10.5 | 100 |
| Platoon blocked, % | | | - | - | | - |
| Mov Cap-1 Maneuver | 742 | 878 | | | 1411 | |
| Mov Cap-2 Maneuver | 742 | - | - | - | - | _ |
| Stage 1 | 869 | | | | - | 1.0 |
| Stage 2 | 946 | - | - | | _ | - |
| | | | | | | |
| Assessments | 14/53 | | 3.175 | | SB | |
| Approach | WB | | NB | | | |
| HCM Control Delay, s | 0 | | 0 | | 0 | |
| HCM LOS | Α | | | | | |
| | | | | | | |
| Minor Lane/Major Mvmt | | NBT | NBR | WBLn1 | SBL | SBT |
| Capacity (veh/h) | 100 | | ARREST | - | 1411 | |
| HCM Lane V/C Ratio | | | | | 199.1 | 1 1 1 2 2 |
| HCM Control Delay (s) | | | 7 | 0 | 0 | |
| | | | | A | A | |
| HCM Lane LOS | | 20.34 | | А | 0 | |
| HCM 95th %tile Q(veh) | | 100 | | - 1 | U | 100 |
| | | | | | | |

| | | 4 | † | - | 6 | 1 |
|-------------------------|-------|------|----------|-------|-----------|------|
| | • | | - | • | | • |
| Lane Group | WBL | WBR | NBT | NBR - | SBL | SBT |
| Lane Configurations | W | | 10 | | | 4 |
| Traffic Volume (vph) | 1 | 2 | 160 | 1 | 1 | 78 |
| Future Volume (vph) | 1 | 2 | 160 | 1 | 1 | 78 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | -2% | | 0% | | | -1% |
| Link Speed (mph) | 10 | | 35 | | | 35 |
| Link Distance (ft) | 415 | | 188 | | | 814 |
| Travel Time (s) | 28.3 | | 3.7 | | | 15.9 |
| Peak Hour Factor | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 | 0.93 |
| Heavy Vehicles (%) | 0% | 0% | 1% | 0% | 0% | 0% |
| Shared Lane Traffic (%) | | | | | | |
| Sign Control | Stop | | Free | | | Free |
| | | | | | | |
| Intersection Summary | OH | | | 3 10 | ST - 1815 | |
| Area Type: | Other | | | | | |

| International Property International Prope | | | | | | | |
|--|--|-----|-----------|-------------|--------|--------|-------|
| ane Configurations araffic Vol, veh/h 1 2 160 1 1 78 tuture Vol, veh/h 1 2 160 1 1 78 tonflicting Peds, #/hr 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Intersection | | | | | | 2 |
| ane Configurations raffic Vol, veh/h 1 2 160 1 1 78 uture Vol, veh/h 1 2 160 1 1 78 uture Vol, veh/h 1 2 160 1 1 78 onflicting Peds, #/hr 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Int Delay, s/veh | 0.1 | | | | | |
| raffic Vol, veh/h atture Volo Ratio atture Volo R | Movement | WEL | WBR | NBT | NBR | SBL | SBT |
| raffic Vol, veh/h 1 2 160 1 1 78 uture Vol, veh/h 1 2 160 1 1 78 conflicting Peds, #/hr 0 0 0 0 0 0 0 1 1 78 conflicting Peds, #/hr 0 0 0 0 0 0 0 1 1 78 conflicting Peds, #/hr 0 0 0 0 0 0 0 1 1 78 conflicting Peds, #/hr 0 0 0 0 0 0 0 1 1 0 0 0 control Channelized - None - | | | | | | | |
| tuture Vol, veh/h conflicting Peds, #/hr conflicting Stop ceal Pedes ceal | | | 2 | | - 9 | 1 | |
| Stage 1 | | - | | | 1 | 1 | |
| ign Control Stop Stop Free Free Free Free Free IT Channelized - None - None - None torage Length 0 - 0 | | | 0 | | | | |
| T Channelized | | | | | 100 | | |
| torage Length | | | | | | | |
| eh in Median Storage, # 0 - 0 - 0 - 0 rade, % -2 - 01 eak Hour Factor 93 93 93 93 93 93 93 93 93 93 93 93 93 | | | | | | - | |
| rade, % | | | | | | | 0 |
| leak Hour Factor 93 93 93 93 93 93 93 93 93 93 93 93 93 | | | | | | | |
| Part | | | | | | | |
| Minist Flow 1 2 172 1 1 84 | | | | | | | |
| Stage 1 | the state of the s | | | | | | _ |
| Stage 1 | MANULLION | | A | 116 | | | 9.1 |
| Stage 1 | | | | | | | |
| Stage 1 | | _ | | | | | |
| Stage 2 86 | Conflicting Flow All | | 173 | 0 | 0 | 173 | 0 |
| Initical Hdwy Stg 1 5 | Stage 1 | | | 000 | | not es | 7 |
| #### Tritical Holland | Stage 2 | | - | - | - | | - |
| ### A Printical Hollowy Stg 1 | Critical Hdwy | | 6 | - | | 4.1 | |
| oflow-up Hdwy | Critical Hdwy Stg 1 | | - | - | _ | - | - |
| collow-up Hdwy 3.5 3.3 - - 2.2 - ct Cap-1 Maneuver 756 884 - 1416 - Stage 1 879 - - - - Stage 2 951 - - - - latoon blocked, % - - - - - lov Cap-1 Maneuver 755 884 - 1416 - lov Cap-2 Maneuver 755 - - - - - Stage 1 879 - - - - - - Stage 2 950 - | Critical Hdwy Stg 2 | 5 | William ! | and the | | | |
| ot Cap-1 Maneuver 756 884 - 1416 - Stage 1 879 Stage 2 951 Idation blocked, % | Follow-up Hdwy | 3.5 | 3.3 | - | - | 2.2 | - |
| Stage 1 879 | | | 884 | | | 1416 | 1 |
| Stage 2 951 | | | - | ~ | - | - | - |
| Idation blocked, % | | | - | 70. | 11 2 | _ | |
| Nov Cap-1 Maneuver | | | | - | - | | |
| Stage 1 | | 755 | 884 | - | | 1416 | |
| Stage 1 879 Stage 2 950 Deproach WB NB SB CM Control Delay, s 9.3 0 0.1 CM LOS A Inot Lane/Major Mymt NBT NBR WBL11 SBL SBT apacity (veh/h) - 836 1416 - CM Lane V/C Ratio - 0.004 0.001 - CM Control Delay (s) - 9.3 7.5 0 CM Lane LOS - A A A | | | | - | | | |
| Stage 2 950 - | | | | 21 | | | 1.00 |
| Deproach WB | | | | | | - | - |
| CM Control Delay, s 9.3 0 0.1 CM LOS A Inor Lane/Major M/mt NBT NBR WBLn1 SBL SBT apacity (veh/h) - 836 1416 - CM Lane V/C Ratio - 0.004 0.001 - CM Control Delay (s) - 9.3 7.5 0 CM Lane LOS - A A A | Stage 2 | 300 | C2 1920 | | | | |
| CM Control Delay, s 9.3 0 0.1 CM LOS A Inor Lane/Major M/mt NBT NBR WBLn1 SBL SBT apacity (veh/h) - 836 1416 - CM Lane V/C Ratio - 0.004 0.001 - CM Control Delay (s) - 9.3 7.5 0 CM Lane LOS - A A A | | | | | | | |
| CM LOS A Inor Lane/Major M/mt NBT NBR Will.n1 SBL SBT apacity (veh/h) 836 1416 - CM Lane V/C Ratio 0.004 0.001 - CM Control Delay (s) - 9.3 7.5 0 CM Lane LOS - A A A | | | | | | | ببيتة |
| Inor Lane/Major Mymt NBT NBR WBLat SBT apacity (veh/h) 836 1416 - CM Lane V/C Ratio 0.004 0.001 - CM Control Delay (s) - 9.3 7.5 0 CM Lane LOS - A A A | HCM Control Delay, s | 9.3 | | 0 | | 0.1 | |
| apacity (veh/h) 836 1416 - CM Lane V/C Ratio 0.004 0.001 - CM Control Delay (s) 9.3 7.5 0 CM Lane LOS - A A A | HCM LOS | Α | | | | | |
| apacity (veh/h) 836 1416 - CM Lane V/C Ratio 0.004 0.001 - CM Control Delay (s) 9.3 7.5 0 CM Lane LOS - A A A | | | | | | | |
| apacity (veh/h) 836 1416 - CM Lane V/C Ratio 0.004 0.001 - CM Control Delay (s) 9.3 7.5 0 CM Lane LOS - A A A | Minor Lane/Major Mont | | NRT | NBR | WB1.n1 | SBL | SBT |
| CM Lane V/C Ratio - - 0.004 0.001 - CM Control Delay (s) - - 9.3 7.5 0 CM Lane LOS - A A A | | | | - | | | |
| CM Control Delay (s) 9.3 7.5 0 CM Lane LOS A A A | | | | - 5 | | | |
| CM Lane LOS A A A | | | | | | | |
| | I The state of the | | | | | | |
| CIM 2001 JOHE MACH | | | - | The section | | | |
| | THOM SOUR FUCE MOT | | 100 | - | U | U | |

| | | 4 | + | - | - | 1 |
|-------------------------|-------|------|----------|------|------|------|
| | | | - 1 | - | | ₩ |
| Lane Group | WEL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Sept. | | 10 | | | 4 |
| Traffic Volume (vph) | 1 | 0 | 190 | 6 | 0 | 103 |
| Future Volume (vph) | 1 | 0 | 190 | 6 | 0 | 103 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | 2% | | 2% | | | -1% |
| Link Speed (mph) | 10 | | 35 | | | 35 |
| Link Distance (ft) | 589 | | 922 | | | 644 |
| Travel Time (s) | 40.2 | | 18.0 | | | 12.5 |
| Peak Hour Factor | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 | 0.90 |
| Heavy Vehicles (%) | 0% | 0% | 1% | 0% | 0% | 0% |
| Shared Lane Traffic (%) | | | | | | |
| Sign Control | Stop | | Free | | | Free |
| Intersection Summary | | | | | | |
| | Other | | | | | - 1 |
| Area Type: | Other | | | | | |

| Intersection | | | | | 811. | |
|--|--------|----------|------------|----------|---------|--------|
| Int Delay, s/veh | 0 | | | | | |
| Movement | WEL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Y | 11011 | 16 | 1 1321 5 | 950 | 4 |
| | 1 | 0 | 190 | 6 | 0 | 103 |
| Traffic Vol, veh/h | 1 | 0 | 190 | 6 | 0 | 103 |
| Future Vol, veh/h | | | | 0 | 0 | 0 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | | | |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | | None | - | None | | None |
| Storage Length | 0 | | _ | | - | _ |
| Veh in Median Storage, # | | - | - 0 | 100 | - | 0 |
| Grade, % | 2 | - | 2 | - | - | -1 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, % | 0 | 0 | 1 | 0 | 0 | 0 |
| Mymt Flow | 1 | 0 | 211 | 7 | 0 | 114 |
| ************************************** | | | | | | |
| | - A | | Children V | 27 | AMERICA | |
| | Minor1 | | Majorf | | Major2 | |
| Conflicting Flow All | 329 | 215 | 0 | 0 | 218 | 0 |
| Stage 1 | 215 | | | - | 100 | |
| Stage 2 | 114 | - | - | - | - | - |
| Critical Hdwy | 6.8 | 6.4 | 1 | | 4.1 | 141 |
| Critical Hdwy Stg 1 | 5.8 | - | - | _ | - | - |
| Critical Hdwy Stg 2 | 5.8 | 1111 | 3. | | | 415 |
| Follow-up Hdwy | 3.5 | 3.3 | _ | - | 2.2 | |
| Pot Cap-1 Maneuver | 646 | 820 | 1 | | 1364 | |
| Stage 1 | 806 | 50,00 | _ | | 1001 | |
| | 904 | The same | | | MINIST. | 1000 |
| Stage 2 | 2011 | | | | | |
| Platoon blocked, % | 010 | 220 | _ | | 1364 | |
| Mov Cap-1 Maneuver | 646 | 820 | | - | | |
| Mov Cap-2 Maneuver | 646 | - | - | - | - | - |
| Stage 1 | 806 | | | | - 4 | |
| Stage 2 | 904 | - | - | - | - | - |
| er Windowskie | | | | | | |
| Anneousk | WB | | NB | TEE | SB | |
| Approach | 10.6 | | 0 | | 0 | 1)= II |
| HCM Control Delay, s | | | 0 | | U | |
| HCM LOS | В | | | | | |
| | | | | | | |
| Minor Lane/Major Mymt | | NBT | NBR | WBLnt | SBL | SBT |
| Capacity (veh/h) | | | | 646 | 1364 | 122 |
| HCM Lane V/C Ratio | | - 100% | - 1167/ | | 1007 | |
| | | 8.2 | | 10.6 | 0 | |
| HCM Control Delay (s) | | | | B | A | |
| HCM Lane LOS | | - | - | | A 0 | |
| HCM 95th %tile Q(veh) | | | | 0 | . 0 | |
| | | | | | | |

| | * | \ | • | + | 1 | 1 | |
|-------------------------|----------|----------|------|----------|------|---------|--|
| | | | , | 1 | • | - | |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | N/F | | | a | 1> | | |
| Traffic Volume (vph) | 0 | 4 | 4 | 195 | 101 | 4 | |
| Future Volume (vph) | 0 | 4 | 4 | 195 | 101 | 1 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Grade (%) | 4% | | | 2% | -2% | | |
| Link Speed (mph) | 35 | | | 10 | 10 | | |
| Link Distance (ft) | 159 | | | 549 | 922 | | |
| Travel Time (s) | 3,1 | | | 37.4 | 62.9 | | |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | |
| Heavy Vehicles (%) | 0% | 25% | 0% | 1% | 0% | 0% | |
| Shared Lane Traffic (%) | | | | | | | |
| Sign Control | Stop | | | Free | Free | | |
| Intersection Summary | | | | | | . No. 1 | |
| Area Type: | Other | Kun Y | | | | | |

| | | | _ | | _ | |
|--|---------|--------|--------|---------|----------------|----------|
| Intersection | | | | | | |
| Int Delay, s/veh | 0.2 | | | | | |
| | | | VI-1 | LHOW | 40.00 | |
| Movement | EBL | EBR | NBL | MET | SBT | SBR |
| Lane Configurations | Y | | | ब | ĵ _e | |
| Traffic Vol, veh/h | 0 | 4 | 4 | 195 | 101 | 1 |
| Future Vol, veh/h | 0 | 4 | 4 | 195 | 101 | 1 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | id toe | None | | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | | T P | 0 | .0 | 12 |
| Grade, % | 4 | - | _ | 2 | -2 | - |
| Peak Hour Factor | 89 | 89 | 89 | 89 | 89 | 89 |
| Heavy Vehicles, % | 0 | 25 | 0 | 1 | 0 | 0 |
| Mymt Flow | 0 | 4 | 4 | 219 | 113 | 1 |
| WWITETION | V | 7 | - 4 | 210 | 110 | |
| | | | | | | |
| Major/Minor N | /linot2 | | Majort | | Major2 | |
| Conflicting Flow All | 341 | 114 | 114 | 0 | - | 0 |
| Stage 1 | 114 | 15 300 | 1 | | la lue | |
| Stage 2 | 227 | - | - | - | - | - |
| Critical Hdwy | 7.2 | 6.85 | 4.1 | | | |
| Critical Howy Stg 1 | 6.2 | _ | - | | _ | - |
| Critical Hdwy Stg 2 | 6.2 | 3 | | 277 | 1.4 | 100 |
| Follow-up Hdwy | 3.5 | 3.525 | 2.2 | - | - | _ |
| Pot Cap-1 Maneuver | 611 | 869 | 1488 | | JE U | |
| Stage 1 | 893 | - | 1,100 | - | - | _ |
| | 775 | 10 1 | 10/2 | O E UE | | 111 |
| Stage 2 | 110 | | - | - | | 11 157.6 |
| Platoon blocked, % | 200 | 800 | 4400 | _ | | |
| Mov Cap-1 Maneuver | 609 | 869 | 1488 | | | |
| Mov Cap-2 Maneuver | 609 | - | - | - | | _ |
| Stage 1 | 890 | 1 | | 1 8 | | |
| Stage 2 | 775 | - | - | - | - | - |
| | | | | | | |
| Approach | EB | | NB | 100 | SB | |
| HCM Control Delay, s | 9.2 | | 0.1 | | 0 | |
| The state of the s | A | | U, t | | U | |
| HCM LOS | A | | | | | |
| | | | | | | |
| Minor Lane/Major Mymt. | - | NBL | NBT | EBLat | SET | SBR |
| Capacity (veh/h) | Will S | 1488 | 1000 | 869 | 11 725 | |
| HCM Lane V/C Ratio | | 0.003 | - | 117.003 | - | _ |
| HCM Control Delay (s) | | 7.4 | 0 | 9.2 | 3 10 . | 5.4 |
| HCM Lane LOS | | A | A | A | - | - |
| The state of the s | | 0 | | 0 | | 1000 |
| HCM 95th %tile Q(veh) | | U | | U | | - |

| | • | _ | > | 1 | — | * | 4 | † | - | 1 | 1 | 1 |
|-------------------------|-----------|-------|----------|-------|----------|----------|------|----------|-----------|------|---------|------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | LUL | 40 | Author 5 | 11100 | A. | T Partie | 1000 | 434 | - Control | | 4 | |
| Traffic Volume (vph) | 12 | 0 | 37 | 7 | 3 | 5 | 73 | 316 | 12 | 9 | 197 | 20 |
| Future Volume (vph) | 12 | 0 | 37 | 7 | 3 | 5 | 73 | 316 | 12 | 9 | 197 | 20 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Grade (%) | 1000 | 0% | | | 0% | | | 5% | | | -2% | |
| Link Speed (mph) | | 25 | | | 25 | | | 25 | | | 25 | |
| Link Distance (ft) | | 330 | | | 456 | | | 339 | | | 344 | |
| Travel Time (s) | | 9.0 | | | 12.4 | | | 9.2 | | | 9,4 | |
| Confl. Peds. (#/hr) | 61 | | 35 | 35 | | 61 | 43 | | 29 | 29 | | 43 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0,95 | 0.95 | 0.95 | 0.95 | 0.95 |
| Heavy Vehicles (%) | 0% | 0% | 0% | 0% | 0% | 20% | 1% | 2% | 0% | 11% | 3% | 0% |
| Parking (#/hr) | 0 | 0 | 0 | 0 | 0 | 0 | | | | | | |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Intersection Summary | 1 1 1 1 1 | | | | | | | | | LOL | _ = 151 | 134 |
| Area Type: | Other | 10160 | | | W N | | | | | | | |

| Intersection | | | 11.5 | -5 | | | | | | | | |
|---|--------|----------|---------|--------|----------|-------|--------|------|------|--------|--------|-------|
| Int Delay, s/veh | 2.3 | | | | | | | | | | | |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NSI. | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | a fi | | | 4 | | | 4 | | | offe | |
| Traffic Vol. veh/h | 12 | 0 | 37 | 7 | 3 | 5 | 73 | 316 | 12 | 9 | 197 | 20 |
| Future Vol. veh/h | 12 | 0 | 37 | 7 | 3 | 5 | 73 | 316 | 12 | 9 | 197 | 20 |
| Conflicting Peds, #/hr | 61 | 0 | 35 | 35 | 0 | 61 | 43 | 0 | 29 | 29 | 0 | 43 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | F 5- | 5 11 | None | = 1 | | None | | - | None | | - 33 | None |
| Storage Length | . An | - | - | - | - | - | - | - | - | - | - | - |
| Veh in Median Storage, # | - | 0 | | | 0 | 140 | | 0 | ES 2 | 100 | 0 | |
| Grade. % | | 0 | - | - | 0 | - | - | 5 | - | * | -2 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, % | 0 | 0 | 0 | 0 | 0 | 20 | 1 | 2 | 0 | 11 | 3 | 0 |
| Mymt Flow | 13 | 0 | 39 | 7 | 3 | 5 | 77 | 333 | 13 | 9 | 207 | 21 |
| WALL STATE OF THE PARTY OF THE | - (10) | | | | | | | | | | | |
| Major/Minor | Minor2 | | | Minorf | | | Majori | | 1 | Major2 | | |
| Conflicting Flow All | 838 | 808 | 296 | 813 | 812 | 430 | 271 | 0 | 0 | 375 | 0 | 0 |
| Stage 1 | 279 | 279 | 45.4 | 523 | 523 | | | | 114 | - 2 | VII 21 | 11114 |
| Stage 2 | 559 | 529 | - | 290 | 289 | - | - | - | - | - | - | - |
| Critical Hdwy | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.4 | 4.11 | - 11 | - F | 4.21 | | 48 |
| Critical Hdwy Stg 1 | 6.1 | 5.5 | - | 6.1 | 5.5 | - | | - | - | - | 16 | - |
| Critical Hdwy Stg 2 | 6.1 | 5.5 | | 6.1 | 5.5 | | 141 | 140 | | 1 | | 1- |
| Follow-up Hdwy | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.48 | 2.209 | - | - | 2.299 | _ | - |
| Pot Cap-1 Maneuver | 288 | 317 | 748 | 299 | 315 | 589 | 1298 | | - | 1136 | | |
| Stage 1 | 732 | 683 | - | 541 | 534 | - | - | - | * | | - | - |
| Stage 2 | 517 | 530 | - | 722 | 677 | 7 | | | | 147 | - | |
| Platoon blocked, % | | | | | | | | - | - | | - | MP. |
| Mov Cap-1 Maneuver | 239 | 270 | 693 | 248 | 269 | 539 | 1245 | 1 | 100 | 1105 | | |
| Mov Cap-2 Maneuver | 239 | 270 | - | 248 | 269 | - | - | - | - | - | - | - |
| Stage 1 | 648 | 649 | 100 | 486 | 479 | | - | - | - | | - | - |
| Stage 2 | 442 | 475 | - | 653 | 643 | - | - | - | - | - | - | - |
| | | | l de la | | | | | | | | | |
| Approach | EB | | | WB | the same | 1 1 1 | NB | | | SB | | |
| HCM Control Delay, s | 13,5 | | | 17.3 | | -1913 | 1.5 | | - 1 | 0.3 | | |
| HCM LOS | В | | | C | | | | | | | | |
| | | | | | | | | | | | III e | |
| Minor Lane/Major Mvmt | | NBL | NBT | NBR | EBLn1 | | SBL | SBT | SBR | | | |
| Capacity (veh/h) | | 1245 | 314 | | 473 | 308 | 1105 | | | | | |
| HCM Lane V/C Ratio | | 0.062 | | _ | 0.109 | 0.051 | 0.009 | - | - | | | |
| HCM Control Delay (s) | | 8.1 | 0 | 9 3 | 13.5 | 17.3 | 8.3 | 0 | | | | |
| HCM Lane LOS | | | | | | | | | | | | |
| | | A 0.2 | Α | - | 0.4 | 0.2 | A | Α | - | | | |

| | • | | 4 | + | 1 | | |
|-------------------------|-------|------|------|----------|--------|------|--|
| | | | , | 1 | Y | | |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | 14 | | | 4 | 10 | | |
| Traffic Volume (vph) | 2 | 21 | 30 | 159 | 77 | 3 | |
| Future Volume (vph) | 2 | 21 | 30 | 159 | 77 | 3 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Grade (%) | 0% | | | 0% | -1% | | |
| Link Speed (mph) | 25 | | | 35 | 35 | | |
| Link Distance (ft) | 189 | | | 644 | 188 | | |
| Travel Time (s) | 5,2 | | | 12.5 | 3.7 | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Heavy Vehicles (%) | 3% | 3% | 3% | 3% | 3% | 3% | |
| Shared Lane Traffic (%) | | | | | | | |
| Sign Control | Stop | | | Free | Free | | |
| Intersection Summary | | No. | | | | | |
| Area Type: | Other | | | | 118.11 | | |

| Intersection | | | | | | |
|--------------------------|--------|-------|--------|-------|----------|---------|
| Int Delay, s/veh | 1.5 | | | | | |
| Management | EBL | EBR | NBL | NBT | SBT | SBR |
| Movement | | LDM | IVOL | | | GOT |
| Lane Configurations | No. | 0.0 | 20 | 159 | 77 | 3 |
| Traffic Vol., veh/h | 2 | 21 | 30 | | | |
| Future Vol, veh/h | 2 | 21 | 30 | 159 | 77 | 3 |
| Conflicting Peds, #/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | 2 5 | None | - | None | | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, # | 0 | | - | | 0 | |
| Grade, % | 0 | - | - | 0 | -1 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, % | 3 | 3 | 3 | 3 | 3 | 3 |
| Mymt Flow | 2 | 23 | 33 | 173 | 84 | 3 |
| TENETIC I TON | | - | | -17 | | |
| | | | | | OTTO THE | |
| | Minor2 | | Majort | | Major2 | |
| Conflicting Flow All | 325 | 86 | 87 | 0 | - | 0 |
| Stage 1 | 86 | - | NEW W | E 5 | | 100 |
| Stage 2 | 239 | - | | - | - | - |
| Critical Hdwy | 6.43 | 6.23 | 4.13 | | = = # | |
| Critical Hdwy Stg 1 | 5.43 | - | | - | - | |
| Critical Hdwy Stg 2 | 5.43 | | | e de | - | 111 |
| Follow-up Hdwy | 3.527 | 3.327 | 2.227 | - | _ | |
| | 667 | 970 | 1503 | | 12:11 | |
| Pot Cap-1 Maneuver | | | 1000 | | - | - |
| Stage 1 | 935 | | | • | | |
| Stage 2 | 798 | - | | | | |
| Platoon blocked, % | | | | - | | - |
| Mov Cap-1 Maneuver | 651 | 970 | 1503 | | 1 | |
| Mov Cap-2 Maneuver | 651 | - | - | - | - | - |
| Stage 1 | 913 | - 4 | | | | |
| Stage 2 | 798 | - | - | - | - | - |
| BY ENDINE MINES | | | | | | |
| | 90.00 | | 8.090 | | 20.00 | |
| Approach | EB | | NB | | SB | |
| HCM Control Delay, s | 9 | | 1.2 | | 0 | |
| HCM LOS | Α | | | | | |
| | | | | | | |
| Minor Lane/Major Mvmt | | NBL | NBT | EBLn1 | SBT | SBR |
| | | | | | 001 | aon |
| Capacity (veh/h) | | 1503 | - | 930 | | |
| HCM Lane V/C Ratio | | 0.022 | - | 0.027 | | _ |
| HCM Control Delay (s) | | 7.4 | 0 | 9 | | |
| HCM Lane LOS | | Α | Α | Α | - | - |
| HCM 95th %tile Q(veh) | | 0.1 | - 1 | 0.1 | - 4 | Llander |
| | | | | | | |

Appendix C

Florida Department of Transportation Corridor LOS Definition

Appendix A: Florida Department of Transportation Roadway Level of Service Definitions



TABLE 6

Generalized Peak Hour Two-Way Volumes for Florida's Rural Undeveloped Areas and

Developed Areas Less Than 5,000 Population¹

12/18/12

| | INTERNO | | LOW PACI | 1111-5-1 | |
|-------|-----------|-------|----------|----------|----|
| | STATE SIG | NALIZ | ZED ART | ERIALS | |
| Lanes | Median | В | C | D | E |
| 2 | Undivided | * | 1,220 | 1,350 | 非非 |
| 4 | Divided | * | 2,790 | 2,890 | 非非 |
| 6 | Divided | * | 4,300 | 4,350 | ** |

INTERPLIPTED ELOW EACH ITIES

Non-State Signalized Roadway Adjustments

(Alter corresponding state volumes by the indicated percent.) Non-State Signalized Roadways - 10%

Median & Turn Lane Adjustments

| | | Exclusive | Exclusive | Adjustment |
|-------|-----------|------------|-------------|------------|
| Lanes | Median | Left Lanes | Right Lanes | Factors |
| 2 | Divided | Yes | No | +5% |
| 2 | Undivided | No | No | -20% |
| Multi | Undivided | Yes | No | -5% |
| Multi | Undivided | No | No | -25% |
| _ | _ | - | Yes | + 5% |

One-Way Facility Adjustment

Multiply the corresponding two-directional volumes in this table by 0.6

BICYCLE MODE²

(Multiply motorized vehicle volumes shown below by number of directional roadway lanes to determine two-way maximum service volumes.)

Rural Undeveloped

| Paved Shoulder/Bicycle | | | | | | | | | | |
|------------------------------|------|-------|--------|--------|--|--|--|--|--|--|
| Lane Coverage | В | C | D | E | | | | | | |
| 0-49% | altr | 120 | 190 | 300 | | | | | | |
| 50-84% | 100 | 200 | 310 | >1,010 | | | | | | |
| 85-100% | 250 | 370 | 1,760 | >1,760 | | | | | | |
| Developed Areas | | | | | | | | | | |
| Paved Shoulder/Bicycle | | | | | | | | | | |
| Lane Coverage | В | C | D | E | | | | | | |
| 0-49% | 3 0 | 220 | 460 | 1,480 | | | | | | |
| 50-84% | 170 | 430 | 1,270 | >1,760 | | | | | | |
| 85-100% | 560 | 1,760 | >1,760 | ** | | | | | | |
| PEDESTRIAN MODE ² | | | | | | | | | | |

(Multiply motorized vehicle volumes shown below by number of directional roadway lanes to determine two-way maximum service volumes.)

| Sidewalk Coverage | В | C | D | E |
|-------------------|-----|-----|-------|--------|
| 0-49% | a)c | oje | 220 | 840 |
| 50-84% | * | 120 | 780 | 1,390 |
| 85-100% | 320 | 940 | 1,560 | >1,820 |

| | | FREEWAY | 'S | |
|-------|-------|---------|--------|--------|
| Lanes | В | C | D | E |
| 4 | 3,020 | 4,510 | 5,490 | 6,300 |
| 6 | 4,510 | 6,720 | 8,220 | 9,720 |
| 8 | 6,040 | 8,970 | 10,960 | 12,970 |

ININTERRUPTED FLOW FACILITIES

Freeway Adjustments

Auxiliary Lanes Present in Both Directions +1,800

UNINTERRUPTED FLOW HIGHWAYS

| |] | Rural Und | leveloped | | |
|-------|-----------|-----------|-----------|-------|-------|
| Lanes | Median | В | C | D | E |
| 2 | Undivided | 440 | 790 | 1,350 | 2,710 |
| 4 | Divided | 2,440 | 3,820 | 4,840 | 5,500 |
| 6 | Divided | 3,680 | 5,730 | 7,280 | 8,240 |
| | | Develope | d Areas | | |
| Lanes | Median | В | C | D | E |
| 2 | Undivided | 820 | 1,550 | 2,190 | 2,990 |
| 4 | Divided | 2,460 | 3,860 | 4,970 | 5,660 |
| 6 | Divided | 3,680 | 5,790 | 7,440 | 8,500 |

Passing Lane Adjustments

Alter LOS B-D volumes in proportion to the passing lane length to the highway segment length

Uninterrupted Flow Highway Adjustments

| Lanes | Median | Exclusive left lanes | Adjustment factors |
|-------|-----------|----------------------|--------------------|
| 2 | Divided | Yes | +5% |
| Multi | Undivided | Yes | -5% |
| Multi | Undivided | No | -25% |

¹Values shown are presented as peak hour two-way volumes for levels of service and are for the automobile/truck modes unless specifically stated. This table does not constitute a standard and should be used only for general planning applications. The computer models from which this table is derived should be used for more specific planning applications. The table and deriving computer models should not be used for corridor or intersection design, where more refined techniques exist. Calculations are based on planning applications of the Highway Capacity Manual and the Transit Capacity and Quality of Service Manual.

Florida Department of Transportation Systems Planning Office www.dot.state.fl.us/planning/systems/sm/los/default.shtm

² Level of service for the bicycle and pedestrian modes in this table is based on number of motorized vehicles, not number of bicyclists or pedestrians using the facility.

^{*} Cannot be achieved using table input value defaults.

^{**} Not applicable for that level of service letter grade. For the automobile mode. volumes greater than level of service D become F because intersection capacities have been reached. For the bicycle mode, the level of service letter grade (including F) is not achievable because there is no maximum vehicle volume threshold using table input value defaults.

Appendix D

Trip Generation Calculations

The Outpost at Lake Cle Elum - Kittitas County, WA

Trip Generation Summary

| | | ITE 3 | Directional Distribution ³ | Sistribution ³ | | | Trips Generated | p |
|---------------------------------------|---------|-------|---------------------------------------|------------------------------------|------------------------|-----|-----------------|-------|
| Land Use | Units 1 | LUC | 드 | Out | Trip Rate ² | п | Out | Total |
| Friday Proposed Use: | | | | | | | | |
| Recreational Homes ² | 50 DU | 260 | 20% | 20% | 13.59 | 340 | 340 | 989 |
| | | | Nev | New Daily Trips Generated == | enerated = | 340 | 340 | 089 |
| Friday AM Peak Hour | | | | | | | | |
| Proposed Use: | | | | | | | | |
| Recreational Homes ² | 50 DU | 260 | 55% | 45% | 0.84 | 23 | 19 | 42 |
| | | | | | | | | |
| | | | New AM Pec | New AM Peak Hour Trips Generated = | senerated = | 23 | 19 | 42 |
| Friday PM Peak Hour | | | | | | | | |
| Proposed Use: | | | | | | | | |
| Recreational Homes | 50 DU | 260 | 26% | 41% | 1.11 | 33 | 23 | 26 |
| | | | | | | | | |
| | | | New PM Pec | New PM Peak Hour Trips Generated = | senerated = | 33 | 23 | 56 |
| · · · · · · · · · · · · · · · · · · · | | | | | | | | |

Votes:

1 DU = Dwelling Unit.

² Daily and AM peak hour thip rafes on a Friday based based on the ratio of weekday to Friday PM peak hour rates in ITE Trip Generation Manual, 11th Edition.

³ Land Use Code, trip rate, and directional splits from the Institute of Transportation Engineers (ITE) Trip Generation Manual, 11th Edition, 2021.

